Road & Bridge Design Publications

Monthly Update – February 2023

Revisions for the month of **February** are listed and displayed below and will be included in projects submitted for the **June** letting. The special detail index from **January** will remain in effect.

E-mail bridge related questions to MDOT-Bridge-Design-Standards@michigan.gov.

Bridge Design Manual

12.07.03: Additional guidance for pin and hanger assembly replacements.

Bridge Design Guides

6.06.05: Updated clear zones for 45-50 mph at 1:6 or flatter slopes, Design Speed to ≥ 65 mph and footnote " * ".

Updates to the MDOT Cell Library, Sample Plans, and other automated tools may be required in tandem with some of this month's updates. Until such updates can be made, it is the designer's/detailer's responsibility to manually incorporate any necessary revisions to notes and plan details to reflect these revisions.

12.07.03

Pins and Hangers (1-24-2022)

The pin and hanger assemblies of cantilever bridges are particularly susceptible to corrosion, and their replacement may have to be included in painting contracts. Region scoping engineers will designate which assemblies will have to be replaced. See Chapter 7 for details.

Where steel beams of adjacent spans are in contact or insufficient expansion length is available between beam ends, consider addressing the closure and the cause of the closure.

If the webs are buckling at closed pin and hanger assemblies, the closure should be addressed.

There are several options to address the closure. Feasibility of various options is dependent on the proposed scope of work. The decision should also be based on the maintenance report and/or observations made during field reviews.

Often, pressure from approaching concrete pavements cause the superstructure to shorten and should be addressed by adding pavement relief joints.

The following repair methodology/criteria is relevant only for redundant structures:

If two pin and hanger assemblies exist between fixed bearings, the closed pin and hanger assembly can be fixed by adding a bolted stay plate and removing the stay plate at the opposing assembly. Substructures should be analyzed for additional loads, where applicable.

If the deck is being replaced, beams may be pulled back to their original location, restoring the opening between beam ends. Other work to the superstructure may be necessary.

12.07.03 (continued)

If necessary, beam ends can be trimmed. To determine the feasibility of trimming, the capacity of the beam must be evaluated for the proposed edge distance between the pin holes and the cut surfaces. If pack rust exists between pin plates of built-up members, employ mechanical means of beam cutting.

If beams are in contact, and cutting or other methods stated above cannot be implemented to relieve the pressure and/or restore the opening between beam ends, an analysis should be performed to ensure that the beams can be left in contact until a project with sufficient scope to address the issue can be constructed.

The assessment and repair of non-redundant (fracture critical) structures should be handled on a case by case basis. It may not be prudent to leave girder ends in contact until a project with sufficient scope can be constructed since web buckling of a single member could have a larger impact on the overall performance of the superstructure.

Generally, the design of new pin and hanger assemblies result in dimensions that are different than those of the existing assemblies. The designer must ensure that the proposed pin and hanger assemblies do not conflict with existing elements and will fit within the confines of the existing superstructure while still meeting all applicable design requirements. (2-21-2023)

New pins shall be stainless steel and used in conjunction with nylon washers and non-metallic bushings. New pin plates/link plates shall use an allowable bearing stress of 0.8 F_y. Non-redundant structures shall use a reduced allowable bearing stress of 0.4 F_y. (12-5-2005)

CLEAR ZONE DISTANCES
(IN FEET FROM EDGE OF DRIVING LANE)

DESIGN SPEED	DESIGN ADT	FILL SLOPES			CUT SLOPES		
		1:6 OR FLATTER	1:5 TO 1:4	1:3	1:3	1:4 TO 1:5	1:6 OR FLATTER
40 mph or Less	under 750	7 - 10	7 - 10	**	7 - 10	7 - 10	7 - 10
	750 - 1500	10 - 12	12 - 14	**	10 - 12	12 - 14	12 - 14
	1500 - 6000	12 - 14	14 - 16	**	12 - 14	14 - 16	14 - 16
	over 6000	14 - 16	16 - 18	**	14 - 16	16 - 18	16 - 18
45-50 mph	under 750	10 - 12	12 - 14	**	8 - 10	8 - 10	10 - 12
	750 - 1500	14 - 16	16 - 20	**	10 - 12	12 - 14	14 - 16
	1500 - 6000	16 - 18	20 - 26	**	12 - 14	14 - 16	16 - 18
	over 6000	20 - 22	24 - 28	**	14 - 16	18 - 20	20 - 22
55 mph	under 750	12 - 14	14 - 18	**	8 - 10	10 - 12	10 - 12
	750 - 1500	16 - 18	20 - 24	**	10 - 12	14 - 16	16 - 18
	1500 - 6000	20 - 22	24 - 30	**	14 - 16	16 - 18	20 - 22
	over 6000	22 - 24	26 - 32*	**	16 - 18	20 - 22	22 - 24
60 mph	under 750	16 - 18	20 - 24	**	10 - 12	12 - 14	14 - 16
	750 - 1500	20 - 24	26 - 32*	**	12 - 14	16 - 18	20 - 22
	1500 - 6000	26 - 30	32 - 40*	**	14 - 18	18 - 22	24 - 26
	over 6000	30 - 32*	36 - 44*	**	20 - 22	24 - 26	26 - 28
≥ 65 mph	under 750	18 - 20	20 - 26	**	10 - 12	14 - 16	14 - 16
	750 - 1500	24 - 26	28 - 36*	**	12 - 16	18 - 20	20 - 22
	1500 - 6000	28 - 32*	34 - 42*	**	16 - 20	22 - 24	26 - 28
	over 6000	30 - 34*	38 - 46*	**	22 - 24	26 - 30	28 - 30

* Where a site-specific investigation indicates a high probability of continuing or higher than expected crashes, or such occurrences are indicated by crash history, the designer may provide clear zone distances greater than 30 feet as indicated. Clear zones may be limited to 30 feet for practicality and to provide a consistent roadway template if previous experience with similar projects or designs indicates satisfactory performance.

** Since recovery is less likely on the unshielded, traversable 1:3 slopes, fixed objects should not be present in the vicinity of the toe of these slopes.