

Draft Traffic Noise Technical Report, US-12/M-51 Interchange Improvements

Prepared for

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List of Acronyms and Abbreviations

ANSI American National Standards Institute

CNE common noise environment

CPBU cost per benefited receptor unit

dB decibel (measure of sound pressure level on a logarithmic scale)

dBA A-weighted decibel (sound pressure level)

DU dwelling unit

DUE dwelling unit equivalent

FHWA Federal Highway Administration

HMA Hot Mix Asphalt

Leq equivalent sound level (energy averaged sound level)

Leq(1h) A-weighted, energy average sound level during a 1-hour period

LOS level of service

MDOT Michigan Department of Transportation

mph miles per hour

NAC noise abatement criteria

NR noise reduction

ROW right of way

ST short-term

TNM Traffic Noise Model

Executive Summary

This noise analysis was conducted to assess the noise impacts associated with the US-12/M-51 intersection improvement project in Niles, MI. The purpose of the proposed project improvements is to improve safety, maintain required capacity, provide operational consistency within the regional US-12 corridor, and adhere to current MDOT design and environmental standards. The project includes improvements to both US-12 and M-51. In addition to the interchange modifications, the project includes intersection and signal improvements, Hot Mix Asphalt (HMA) mill & overlay, pavement repairs, and sidewalk work.

FHWA defines Type I projects as Federal highway projects that result in a highway in a new location, a physical alteration of an existing highway that significantly changes either horizontal or vertical alignment, or an increase to the number of through lanes. This noise study is required for this project because the interchange/intersection improvement would require a significant change in the elevation of the US-12 travel lanes approaching the new US-12/M-51 intersection, satisfying the definition of a Type I project. Thus, the entire project area needs to be studied as a Type I project and assessed for potential noise impacts and mitigation options.

This noise study included on-site noise measurements in the project vicinity. Measurements were conducted in September 2021 to validate noise models. A total of twelve short-term (ST) noise measurements were conducted at representative locations across the project area.

A predictive noise model was developed in the FHWA Traffic Noise Model (TNM) version 2.5 and validated against these field measurements. Noise-sensitive receptors were then identified and classified with existing and future levels calculated in TNM 2.5. Predicted noise levels were then checked against FHWA and MDOT standards to determine traffic noise impacts in the study area. Noise abatement for these impacts was analyzed using TNM and assessed per MDOT feasibility and reasonableness criteria.

The analysis identified a total of twelve defined Common Noise Environments (CNEs). Of these twelve established CNEs, seven were identified to contain impacted receptors. Abatement in the form of noise walls were considered in each impacted CNE but none were determined to be reasonable and feasible in accordance with MDOT policy. A summary of these findings is presented in Table ES-1 and discussed in more detail in the body of the report.

Table ES-1 Summary of Project Impacts and Proposed Noise Abatement

CNE	Description/Location	Existing Impacts	Future Impacts	Noise Abatement Recommendation	
CNE-1	Single-Family Homes	2	9	Not Recommended	
OIVE-1	North of US-12, East of M-51		3	Not recommended	
CNF-2	Commercial, Single-Family Homes	0	0	No Impacts	
ONL-Z	North of Brandywine St., East of M-51	0	0	140 IIIIpacis	
CNE-3	Cemetery, Baseball Park	8	8	Not Recommended	
OIVE-0	North of Silverbrook St., East of M-51	0	0	Not recommended	
CNE-4	Single-Family Homes, Commercial	6	6	Not Recommended	
ONE 4	North of Cherry St., East of M-51			Tet Recommended	
CNE-5	Single-Family Homes	4	4	Not Recommended	
OIVE-0	North of Main	7	7		
CNE-6	Commercial, Single-Family Homes	0	0	No Impacts	
OIVE-0	North of Silverbrook St., West of M-51	0	0	TTO IIIIpaoto	
CNF-7	Commercial	0	0	No Impacts	
CINL-7	North of Fort St., West of M-51	0	0	No impacts	
	Commercial, Single-Family Homes, Public		1		
CNE-8	Park	1		Not Recommended	
	North of US-12, West of M-51				
CNE-9	Single-Family Homes	3	3	Not Recommended	
OITE 0	South of US-12, West of 3rd St.			Hot Recommended	
CNF-10	Commercial	0	0	No Impacts	
5.1E 10	South of Bell St., West of M-51		"	110 mpaoto	
CNE-11	Commercial, Single-Family Homes	0	0	No Impacts	
0.42 11	South of Bell St., East of M-51	"	"	140 IIIIpaots	
CNE-12	Single-Family Homes	6	6	Not Recommended	
O14L-12	South of US-12, East of M-51			Not Recommended	

1. Introduction and Project Description

1.1 Project Description

The project is located on M-51 from south of Chestnut Lane northerly to M-60BR and on US-12 from west of 3rd Street easterly to east of M-51, including the associated ramps at US-12 and M-51 in Niles Charter Township and the city of Niles in Berrien County. The project area and ramps are shown in Figure 1-1. The primary objective of the project is to remove the grade-separated US-12/M-51 interchange and replace it with a signalized intersection as shown in Figure 1-2. Additional work associated with the larger project area includes intersection and signal improvements, HMA mill & overlay, pavement repairs, and sidewalk work. The proposed US-12/M-51 interchange modifications qualify the project as Type I and thus require a full noise analysis. Although these qualifying improvements are localized to the interchange area, FHWA and MDOT policy requires the noise analysis to assess the entire project area for noise impacts and potential noise abatement. All noise-sensitive properties with a defined outdoor use area within approximately 500 feet of the project roadways were evaluated for noise impacts and potential noise abatement in accordance with MDOT policy.

The areas along US-12 west of the interchange include several residential properties, a church, and a nature park on 3rd St. East of the interchange north and south of US-12, there are residential properties on Oakdale Ave. and Greendale Ave. respectively. The area along M-51 between the interchange and Chestnut Lane to the south is primarily developed as commercial properties with some residential and undeveloped areas. The area along M-51 between the interchange and M-60BR (Oak Street) to the north includes several areas with residential land uses (South St., Ferndale Blvd., Brandywine St., Lambert St., Cherry St. Maple St., and Hickory St.), hotels, a ballpark, a cemetery, a few fast-food restaurants with outdoor seating areas, and vacant land.

In addition to the above-described areas within the project area are construction zones beyond the main project area where temporary cross-over lanes will be constructed at the beginning of the project that will be removed at project completion. These areas will be evaluated for possible construction noise impacts only. These construction areas are also shown in Figure 1-1.

1.2 Description of Alternatives

This project includes one future build alternative to be evaluated:

Future build (includes all proposed improvements and projected traffic volumes for Year 2043)

Figure 1-1 Project Overview

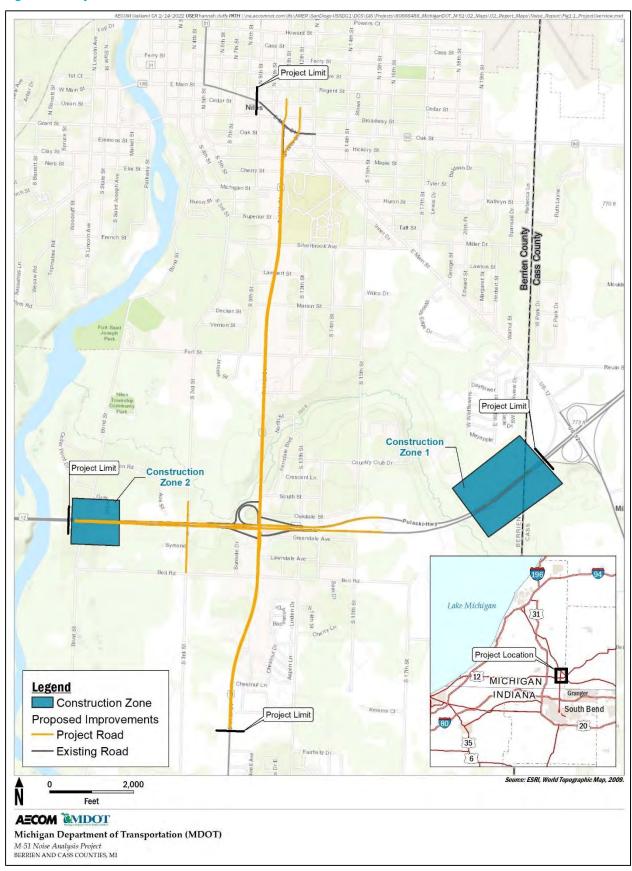




Figure 1-2 Proposed US-12/M-51 Intersection Improvements

2. Traffic Noise Concepts

The following glossary of acoustical terms is intended to help frame the discussion of project-generated noises and their potential effects on neighboring communities in the project area.

2.1 Glossary of Acoustical Terms

Noise: Whether something is perceived as a noise event is influenced by the type of sound, the perceived importance of the sound, and its appropriateness in the setting, the time of day, and the type of activity during which the noise occurs, and the sensitivity of the listener. Local jurisdictions may have legal definitions of what constitutes "noise" and such environmental parameters to consider.

Sound: For this analysis, sound is a physical phenomenon generated by vibrations that result in waves that travel through a medium, such as air, and result in auditory perception by the human brain.

Frequency: Sound frequency or "pitch" is measured in hertz (Hz), which is a measure of how many times each second the crest of a sound pressure wave passes a fixed point. For example, when a drummer beats a drum, the skin of the drum vibrates a number of times per second. When the drum skin vibrates 100 times per second, it generates a sound pressure wave that is oscillating at 100 Hz, and this pressure oscillation is perceived by the brain as a tonal pitch of 100 Hz. Sound frequencies between 20 and 20,000 Hz are within the range of sensitivity of the best human ear.

Amplitude or Level: Sound levels are measured in decibels (dB) using a logarithmic scale. A sound level of zero dB is approximately the threshold of human hearing and is barely audible under extremely quiet listening conditions. Normal speech has a sound level of approximately 60 dB. Sound levels above approximately 110 dB begin to be felt inside the human ear as discomfort and eventually as pain at 120 dB and higher levels. The minimum change in the sound level of individual events that the average human ear can detect is about 1 to 2 dB. A 3 to 5 dB change is readily perceived. A change in sound level of about 10 dB usually is perceived by the average person as a doubling (or if decreasing by 10 dB, halving) of the sound's loudness. Table 2-1 shows typical indoor and outdoor sounds and their corresponding dB levels, arranged on what often is referenced as an "acoustic thermometer" to show relative loudness.

Sound pressure: Sound level usually is expressed by reference to a known standard. This report refers to sound pressure level, which is expressed on a logarithmic scale with respect to a reference value of 20 micropascals. Sound pressure level depends not only on the power of the source, but also on the distance from the source and the acoustical characteristics of the space surrounding the source.

A-weighting: Sound from a tuning fork contains a single frequency (a pure tone), but most sounds heard in the environment do not consist of a single frequency; instead, they are composed of a broad band of frequencies, differing in sound levels. The method commonly used to quantify environmental sounds consists of evaluating all frequencies of a sound according to a weighting system that reflects the typical frequency-dependent sensitivity of average healthy human hearing. This is called "A-weighting," and the measured decibel level is referred to as A-weighted decibels (dBA).

Equivalent sound level: Environmental noise levels vary continuously and include a mixture of noise from near and distant sources. A single descriptor, energy-average sound level during a measured time interval (L_{eq}), may be used to describe such sound that is changing in level from one moment to another. L_{eq} is the energy-average sound level during a measured time interval. This is the "equivalent" constant sound level that would have to be produced by a single, steady source to equal the acoustic energy contained in the fluctuating sound level measured.

Insertion loss (IL): The IL is the reduction in noise level at a location from noise abatement means, placed in the sound path between that location and a sound source.

2.2 Fundamentals of Traffic Noise Assessment and Control

Sound Propagation

Atmospheric conditions (e.g., wind, temperature gradients, humidity) can change how sound propagates over distance and can affect the level of sound received at a given location. The degree to which the ground surface absorbs acoustical energy also affects sound propagation. Sound traveling over an acoustically absorptive surface (e.g., grass) attenuates at a greater rate than sound traveling over a hard surface (e.g., pavement, expanses of open water). When located near either the sound source or the listener position, physical barriers (e.g., naturally occurring ridgelines or buildings, and other topography that block the line-of-sight between a source and receiver) also increase the attenuation of sound over distance.

Multiple Sound Sources

Because sound pressure levels in decibels are based on a logarithmic scale, they cannot be added or subtracted in an arithmetic fashion. Therefore, sound pressure level dB are logarithmically added on an energy summation basis. In other words, adding a new noise source to an existing noise source, both producing noise at the same level, does not double the noise level. Instead, if the difference between two noise sources is 10 dBA or more, the louder noise source dominates, and the resultant noise level is equal to the noise level of the louder source. In general, if the difference between two noise sources is 0 to 1 dBA, the resultant noise level is 3 dBA higher than the louder noise source, or both sources if they are equal. If the difference between two noise sources is 2 to 3 dBA, the resultant noise level is 2 dBA above the louder noise source. If the difference between two noise sources is 4 to 10 dBA, the resultant noise level is 1 dBA higher than the louder noise source.

How Noise is Measured

Sound can vary over an extremely large range of amplitudes. The decibel (dB) is a logarithmic unit that is the accepted standard unit for measuring the amplitude of sound because it accounts for these large variations in amplitude and reflects the way people perceive changes in sound amplitude. Different sounds may have different frequency content. Frequency content of a sound refers to its tonal quality or pitch. When describing sound and its effect on a human population, A-weighted (dBA) sound levels are typically used to account for the response of the human ear. The term "A-weighted" refers to a filtering of the noise signal to emphasize frequencies in the middle of the audible spectrum and to de-emphasize low and high frequencies in a manner corresponding to the way the human ear perceives sound. This filtering network has been established by the American National Standards Institute (ANSI). The A-weighted noise level has been found to correlate well with peoples' judgments of the noisiness of different sounds and has been used for many years as a measure of community noise. Table 2-1 illustrates sound pressure levels in dBA of various sound sources between 0 dBA (threshold of hearing) and 120 dBA (threshold of

pain). An increase of 3 dBA in noise level can barely be perceived, while an increase of 5 dBA is readily noticeable and considered a significant noise increase. A 10 dBA increase corresponds to a subjective doubling of loudness. A relationship between changes in noise level and loudness is indicated in Table 2-2. Since noise fluctuates from moment to moment, it is common practice to condense the noise level over a specified period of time into a single number called the Equivalent Noise Level (Leq). Many surveys have shown that the Leq properly predicts annoyance, and thus this metric is commonly used for noise measurements, prediction, and impact assessment.

Table 2-1 Common Indoor and Outdoor Noise Levels

Common Outdoor Noise Levels Noise Level	Noise Level (A-weighted decibels)	Common Indoor Noise Levels
	110	Rock Band
Jet Flyover at 1000 feet	100	Inside Subway Train (NY)
Gas Lawn Mower at 3 feet		
Diesel Truck at 50 feet	90	Food Blender at 3 feet
Noisy Urban Daytime	80	Garbage Disposal at 3 feet
Gas Lawn Mower at 100 feet	70	Vacuum Cleaner at 10 feet
Commercial Area		Normal Speech at 3 feet
	60	
		Large Business Office
Quiet Urban Daytime	50	Dishwasher Next Room
Quiet Urban Nighttime	40	Small Theater
Quiet Suburban Nighttime		Library
	30	
Quiet Rural Nighttime		Bedroom at Night
	20	
		Broadcast & Recording Studio
	10	
	0	Threshold of Hearing

Source: Adapted from Guide on Evaluation and Attenuation of Traffic Noise, AASHTO-1974

Table 2-2 Relationship between Changes in Noise Level and Perceived Loudness

Increase (or Decrease) in Noise Level	Loudness Multiplied (or Divided) by
3 decibels	1.2
6 decibels	1.5
10 decibels	2
20 decibels	4

How Highway Noise is Generated

Highway noise is generated from three primary sources: tire/pavement noise, engine noise, and exhaust noise. Tire/pavement noise is the noise generated by the rubber tires rolling over the pavement surface and may vary in intensity and character depending on the type and condition of both the tires and the pavement. For automobiles and light trucks traveling at typical highway speeds (over about 50 miles per hour [mph]), tire/pavement noise is generally the dominant noise source. For medium and heavy trucks (like large commercial delivery vehicles and long-haul tractor-trailers) engine and exhaust noise also contribute to the noise that they produce. At typical highway speeds, one large truck can produce as much noise energy as ten automobiles. How highway noise is experienced at nearby homes is controlled by a number of factors, including: the total number of vehicles on the highway, the percentage of large trucks, the average speed of the vehicles, the distance to the highway, obstructions blocking the view of the highway, and meteorological conditions. Generally speaking, the more vehicles, the higher percentage of large trucks or the closer one is to the highway, the greater the noise will be. Intervening obstructions, either manmade (buildings,

walls, berms) or natural (such as intervening terrain) will reduce noise levels. Foliage and vegetation can reduce noise levels, but it must be dense (completely obscuring the view of the highway) and thick (on the order of 50 to 100 feet) to make a noticeable difference.

How Highway Noise Can Be Reduced

Highway noise can be reduced in several ways. Here are some of the most recognized:

Traffic Controls

The faster vehicles travel, and the higher percentage of large trucks, the louder the noise. Reduced speed limits, or more rigorously enforced existing speed limits, and heavy truck restrictions will reduce noise levels. However, the implementation of such measures is often politically difficult for the sake of lower noise levels alone.

Land Use Controls:

Perhaps the most common sense and fiscally responsible solution to highway noise, and one favored by most highway agencies is to restrict the development of lands near highways. Restricting development of land near new highway corridors to non-noise sensitive land uses, such as commercial or industrial activities can eliminate most noise problems. However, this approach is not suitable for circumstances when land near existing or future highways has already been developed for residential land use.

Quieter Vehicle Noise Sources

Quieter vehicles mean less highway noise. For automobiles, this means quieter tires (since tire/pavement noise is the dominant noise source). For large trucks, the EPA has established standards for maximum noise levels for new and in-use trucks. The maximum noise levels for new trucks are lower than those for some older trucks, so as old trucks are phased out and replaced with newer ones the noise produced by the average truck may go down.

Noise Barrier Walls and Berms

Noise barriers, both structural walls and earthen berms, are often constructed specifically for the purpose of reducing highway noise levels. Noise barriers can be very effective for reducing noise levels at nearby homes, often reducing noise levels by as much as 10 decibels at the closest homes (a perceived halving of loudness). Noise barriers can be expensive to build, on the order of \$2 million per mile. Because of their cost, the construction of noise barriers is often restricted to large highway improvement or construction projects. Some jurisdictions; however, are quite active in constructing "retrofit" noise barriers on existing highways.

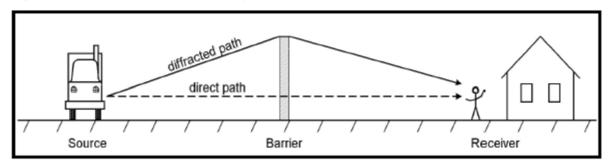
Quieter Pavements

It has long been recognized that some pavement types tend to be quieter than others. White concrete pavement, for example, is typically louder than asphalt blacktop. White concrete with tining (grooves cut into the pavement surface) is louder still. However, white concrete pavement (also known as Portland Concrete Cement, or PCC) is thought to be more durable, and perhaps safer than blacktop pavements (due to better skid resistance and drainage). There is also considerable concern that the low noise advantages of some blacktop pavements may diminish over time. As the tiny "nooks and crannies" in the blacktop pavement that give it acoustical absorption may fill up with silt and sand or become compressed over time, the acoustical benefits are reduced. The quest for quiet, safe, and durable highway pavements is currently the focus of a considerable amount of research.

How Noise Barriers Work

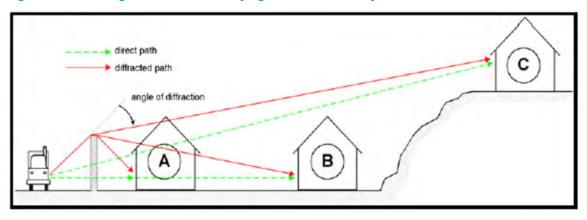
Noise barriers reduce noise levels by interrupting or lengthening the path that the noise takes between the source and the receiver. To be effective at reducing noise, noise barriers must be able to block the "line of sight" between the object producing the noise (like vehicles on the highway) and the person subjected to the noise (like residents living near the highway). The amount that the noise will be reduced is related to the path length difference between the "direct path" that the uninterrupted sound would take between the source and receiver (with no barrier) and the "diffracted path" that the sound must take going over or around the barrier, as illustrated in Figure 2-1

Figure 2-1 Simple Noise Barrier Geometry



Noise barriers may work better for some homes than for others. In Figure 2-2, below, home "A" is relatively close to the highway where the noise barrier can provide a large path length difference between the direct and diffracted paths, resulting in a substantial noise reduction (perhaps as much as 10 to 15 decibels). Home "B" is further from the barrier and the path length difference is not as great, resulting in less noise reduction (perhaps 7 to 10 decibels). Home "C" is even further from the highway and also elevated above the highway grade, providing an even smaller path length difference (resulting in a noise reduction of perhaps 3 to 5 decibels). In general, for a given barrier height and location, the further the receiver is from the barrier or the higher the receiver is elevated, the smaller the path length difference (or angle of diffraction) and the smaller the resulting noise reduction.

Figure 2-2 Path Length Difference for Varying Receiver Geometry



2.3 Regulatory Overview

2.3.1 Federal Regulations

The FHWA noise policy is contained within The Code of Federal Regulations, Title 23, Part 772 (23 CFR 772) which provides procedures for preparing operational and construction noise studies and evaluating noise abatement considered for federal and federal-aid highway projects. The code was recently updated in July of 2010. Under the current version of 23 CFR 772.5, projects are categorized as Type I, Type II, or Type III projects. The FHWA defines a Type I project as a proposed federal or federal-aid highway project for the construction of a highway on a new location, the physical alteration of an existing highway which significantly changes either the horizontal or vertical alignment, or increases the number of through-traffic lanes. The proposed project is a Type I project as defined by the FHWA.

Type I projects include those that create a completely new noise source, as well as those that increase the volume or speed of traffic or move the traffic closer to a receptor. Type I projects include the addition of an interchange, ramp, auxiliary lane, or truck-climbing lane to an existing highway, or the widening of an existing ramp by a full lane width for its entire length. Projects unrelated to increased noise levels, such as lighting, signing, and landscaping, are not normally considered Type I projects.

Under 23 CFR 772.13, noise abatement must be considered for Type I projects if the project is predicted to result in a traffic noise impact. In such cases, 23 CFR 772 requires that the project sponsor "consider" noise abatement before adoption of the final NEPA document. This process involves identification of noise abatement measures that are reasonable, feasible, and likely to be incorporated into the project, and of noise impacts for which no apparent solution is available.

Traffic noise impacts, as defined in 23 CFR 772.5, occur when the design year condition noise levels approach or exceed the noise abatement criteria (NAC) specified in 23 CFR 772, or design year condition noise levels create a substantial noise increase over existing noise levels. 23 CFR 772 does not specifically define the terms "substantial increase" or "approach"; these criteria are defined in the MDOT Noise Analysis and Abatement Handbook (July 13, 2011), as described in the following section.

Table 2-3 summarizes the FHWA NAC corresponding to various defined land use activity categories. Activity categories and related traffic noise impacts are determined based on the actual land use in each area.

In identifying noise impacts, primary consideration is given to exterior areas of frequent human use. Interior noise impacts will only be addressed for land uses listed with Activity Category D.

Table 2-3	FHWA Noise A	Abatement (Criteria

Activity Category	Activity Criteria		,		Evaluation Location	Activity description
	Leq(h) L10(h)					
A	57	60	Exterior	Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose.		
В	67	70	Exterior	Residential		
С	67	70	Exterior	Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, day care centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreation areas, Section 4(f) sites, schools, television studios, trails, and trail crossings.		
D	52	55	Interior	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or nonprofit institutional structures, radio stations recording studios, schools, and television studios.		
E	E 72 75		Exterior	Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in A-D or F.		
F	1			Agriculture, airports, bus yards, emergency services, industrial, logging, maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing.		
G				Undeveloped lands that are not permitted.		

¹ Either Leq(h) or L10(h) (but not both) may be used on a project.

2.3.2 State Regulations and Policies

MDOT has published the noise policy which provides guidelines in the analysis of highway traffic noise and the evaluation of noise abatement measures. Effective July 13, 2011, the MDOT *Highway Noise Analysis and Abatement Handbook* (hereafter referred to as "the MDOT handbook") also includes current policies, procedures, and practices to be used by agencies that sponsor new construction or reconstruction of federal or federal-aid highway projects. The MDOT noise handbook defines that a noise impact occurs when the sound level approaches or exceeds the assigned NAC level for a specific category, which is defined as an Leq(h) sound level 1 dBA less than the NAC identified in 23 CFR 772. This means that for an Activity Category B land use (residential), a peak hour noise level of 66 dBA is considered to approach the NAC of 67 dBA and is identified as an impact. The MDOT noise handbook defines a noise increase as substantial when the predicted traffic noise levels with project implementation exceed existing noise levels by 10 dBA. The MDOT noise handbook provides detailed technical

² The Leg(h) and L10(h) Activity Criteria values are for impact determination only, and are not design standards for noise

³ Includes undeveloped lands permitted for this activity

guidance for the evaluation of highway traffic noise. This includes field measurement methods, noise modeling methods, and report preparation guidelines. In addition to the NAC criteria above, the MDOT noise handbook also specifies the following definitions and policies:

Benefited Receptor is the recipient of an abatement measure that receives a noise reduction at or above the minimum threshold of 5 dBA.

Feasible Noise Abatement Measure is an abatement measure that is acoustically feasible and meets engineering requirements for constructability. A noise abatement measure is considered feasible when it can provide at least a 5 dBA reduction to at least 75% of impacted noise receptors and meets constructability, safety, access, utility, and drainage requirements.

Reasonable Noise Abatement Measure is an abatement measure that has been determined to be cost-effective if it costs at or below the allowable cost per benefited receptor unit (CPBU) of \$49,301.00 and is considered acceptable to the majority of residents and property owners who benefit from the noise abatement. The MDOT design year attenuation requirement requires that a minimum of one benefited receptor achieve at least a 10 dBA noise reduction and that at least 50% of benefited receptors achieve a 7 dBA reduction.

3. Methods of Noise Analysis

3.1 Defining Area or Potential Impact

The extent of the noise study analysis area should include all receptors potentially impacted by the project. The FHWA does not establish a fixed distance to define the noise impact analysis area. Historically, absolute noise impacts (those areas with noise levels approaching or exceeding the NAC – 66 dBA for residential land uses) rarely exist beyond about 500 feet from the roadway. The MDOT noise handbook defines the study zone to be a minimum of 500 feet, including all noise-sensitive receptors on all sides of the highway. If an impact is identified at 500 feet, the next closest receptor would need to be analyzed until a distance where impacts are no longer identified is reached. If no receptors are located within the 500-foot zone, then the closest receptor(s) should be analyzed.

3.2 Field Measurement Procedures

Several field noise measurements were conducted for this project. In general, the noise measurement procedures in the field follow recommended standard procedures, including those outlined in the FHWA's Measurement of Highway Related Noise, May 1996, and the MDOT noise handbook. Specifically, the following practices and procedures were used.

The short-term noise measurements (typically 15-25 minutes) were conducted at actual or representative receptor locations and were used primarily to validate the noise prediction model (at locations where traffic noise was dominant). Short-term noise measurements were generally conducted at exterior areas of frequent human use and were only conducted during periods of free-flowing traffic, dry roadways, and low to moderate wind speeds (less than 12 mph to avoid extraneous wind noise).

No long-term noise measurements were conducted for this study due to inclement weather.

Only ANSI (American National Standards Institute) Class I sound level meters were used for short-term measurements. The meters were subjected to a field calibration check before and after each measurement period. Calibration certificates for each meter used in the Project can be found in Appendix A.

Concurrent traffic counts (classified in auto, medium and heavy trucks, buses, and motorcycles) for the acoustically dominant road were conducted for each short-term measurement. Traffic was videotaped during the measurements to be subsequently counted. The traffic counts can be found in Table 3-3.

All field data were recorded on field data sheets, which included the time, name and location of the measurement, instrument information, observed meteorological data, field calibration results, a measurement site diagram, GPS coordinates, and notes regarding the dominant noise sources and any other observed acoustically relevant events (such as aircraft over-flights, emergency vehicle pass-bys, etc.). Field sheets and photographs of measurement sites can be found in Appendix A.

3.3 Analysis Objectives

The purpose of this noise analysis report is to identify, and document potential noise impacts associated with the proposed future Project and to identify feasible and reasonable abatement. The general analysis procedure for the Project noise study includes the following steps:

- Review Project Description: Review the project description and project data to be analyzed and collect additional required data (including roadway design files, existing and future traffic data, land use data, etc.). Consider all alternatives, design options, and construction phasing scenarios. This information is presented in Section 1 of this report.
- 2. **Identify Regulatory Framework:** Investigate and establish the regulatory framework to be followed for the noise analysis, including federal, state, and local regulations and ordinances applicable to the Project. This information is presented in Section 2 of this report.
- 3. Noise Analysis Methodology and Establish Existing Land Use and Noise Environment: Investigate and document the existing noise environment for the Project area, including existing noise-sensitive land uses and existing noise levels in the Project area. These were accomplished with a careful review of local zoning information, review of aerial photography, and a site visit to the Project area. This information is presented in Section 3 of this report.
- 4. Predict Future Noise Levels and Assess Noise Impacts: Future noise levels at noise-sensitive land uses for the future build alternative are predicted using the FHWA TNM Version 2.5. For each alternative, future noise levels (as well as increases in future noise levels over existing noise levels) are assessed for compliance with the identified noise impact criteria and quantify resulting noise impacts. This information is presented in Section 4 of this report.
- 5. **Evaluate Noise Abatement:** Where noise impacts are identified, evaluate potential noise abatement measures. Abatement measures are evaluated for feasibility and reasonableness according to FHWA and MDOT standards. This information is presented in Section 5 of this report.
- 6. **Construction Noise Considerations:** Analyze potential construction noise impacts and discuss available abatement options. This information is presented in Section 6 of this report.
- 7. **Information for Public Officials:** Provide or identify appropriate information for local public officials to help avoid future noise impacts. This information is presented in Section 7 of this report.

A more detailed accounting of the specific procedures involved in each of the above analysis steps is provided in the indicated report section.

3.4 Selection of Noise-Sensitive Receptors

In general, modeled noise-sensitive receptors are identified to represent potentially impacted land uses within the Project area. A common noise environment, or CNE, is generally defined as a group of receptors within the same Activity Category in Table 2-3 that are exposed to similar noise sources and levels; traffic volumes, traffic mix, and speed; and topographic features. Generally, common noise environments occur between two secondary noise sources, such as interchanges, intersections, and/or cross-roads. The delineated CNEs for this Project are described in Section 3.9.2 of this report. Within each CNE, representative noise measurements and noise prediction locations are identified. Typically, each CNE would have one short-term measurement location and multiple noise prediction locations. The number and locations of the receptors (measurement and modeling locations) within each CNE are selected to adequately represent all of the noise-sensitive property units (dwellings) within that CNE, and these properties may include Activity Categories A through E and G in Table 2-3 (including residential, noise-sensitive commercial, parks, schools, hotels, and undeveloped lands.). Activity Category F (agriculture, retail, industrial, transportation, and utilities), may still be located within a CNE, but would be considered a noise-compatible land use and would not require noise analysis. For residential properties, more-isolated residences would generally be modeled as individual receptors, while residences in multi-family buildings and dense neighborhoods may be modeled with one modeled receptor location representing multiple dwelling units or homes (receptors).

All noise prediction locations are placed to represent an exterior area of frequent human use of the receptor. For residential properties, this would normally be an exterior activity area between the structure and the proposed project roadway, such as a pool, patio, or play area.

3.5 Loudest Hour Noise Conditions

When determining noise impacts, traffic noise predictions must be made for the loudest noise hour (generally during level of service [LOS] C or D with high heavy truck volumes and speeds close to the posted speed limit or design speed). The loudest hour noise is typically either the peak vehicular truck hour or the peak vehicular volume hour (with LOS A through D conditions).

3.6 Noise Abatement Requirements

According to FHWA policy and the MDOT noise handbook, once a noise impact has been identified, feasible and reasonable noise abatement measures must be considered. For noise abatement, primary consideration is given to the exterior areas of frequent human use.

When traffic noise impacts are identified, noise barrier walls, at a minimum, are required to be considered. In addition to noise walls, other abatement elements may also be considered, if appropriate and applicable, including the following:

- Traffic management measures.
- Alteration of horizontal and vertical alignments.
- Acquisition of property to serve as a buffer to preempt development that would be adversely
 impacted by traffic noise; and
- Noise insulation (NAC D Only).

When noise barriers are considered, a noise barrier design analysis must show that the barrier is feasible. This typically requires that the barrier provides a minimum required level of noise reduction. According to the MDOT noise handbook, feasible noise barriers must provide at least 5 dBA of noise reduction to at least 75% of impacted receptors. In addition to meeting minimum noise reduction requirements, noise barriers must also meet engineering and constructability feasibility requirements in terms of safety, property and emergency access, drainage control, overhead and underground utility clearance, and other issues.

Noise barrier reasonableness is generally related to cost-effectiveness and benefited receptors. The MDOT noise handbook expresses barrier cost-effectiveness by a quotient formula called the Cost Per Benefited Receptor Unit (CPBU), which divides the total square-foot-cost of the barrier (at a rate of \$45.00/ft²) by the number of benefitted dwelling units. To maintain reasonableness, the total CPBU cannot exceed \$49,301.00, (the total allowable cost established by MDOT for FY 2021). Barriers must also achieve the MDOT noise reduction design goal of 10 dBA reduction for at least one benefited receptor, and 7dBA reduction for at least 50% of benefitted receptors.

If noise barriers are determined to be reasonable and feasible as defined above, then the viewpoints of property owners and residences should be taken into consideration. Approval by a simple majority (greater than 50%) of all responding benefited owners and residences is needed to implement noise abatement. Public votes should occur during final design and could happen during the Context Sensitive Design aesthetic public input phase.

3.7 Noise Modeling Methodology

Future build noise levels, along with existing noise levels, were predicted using FHWA TNM Version 2.5, the most recent version available at the time of the analysis. All conventional modeling techniques and recommendations for TNM by both FHWA and MDOT were implemented. These included the following modeling procedures and conventions:

- TNM roadways were generally modeled as bundled roadways with no more than three lanes represented by a single modeled roadway.
- All roadway pavement types were modeled as "Average".

- Traffic speeds and volumes for peak traffic hour as provided in the traffic data were modeled to predict worst-case noise levels. Traffic speeds and volumes used in this analysis were based on the predicted traffic data included in Table 3-1.
- Existing terrain lines (topography) and buildings were modeled where appropriate.
- All TNM inputs and models runs were reviewed for accuracy by an independent noise analyst.
- Sample TNM input/output files for this project provided in Appendix B
- All TNM model runs are available upon request

3.8 Project Traffic Data

Predicted traffic data for the existing and Future Build were provided by MDOT. Existing traffic data from 2018, the most recent available, and Future Build data for year 2043 were used in the study. AM and PM peak values were evaluated; however, it was determined that combined AM peak values were greater and therefore were used in the loudest hour noise analysis. A summary of the traffic data used for this analysis can be found in Table 3-1.

Table 3-1 Existing and Future Peak Hour Traffic Volumes

	Existing Traffic (AM Peak)									
		M-51				US-12				
	M-51 Nort	h of US-12	M-51 South of US-12		US-12 East of M-51		US-12 West of M-51			
	NB	SB	NB	SB	EB	WB	EB	WB		
Speed (mph) ¹	50	50	50	50	55	55	55	55		
Total	965	782	1266	894	753	335	585	550		
Auto and Light Trucks	927	768	1216	877	632	277	492	483		
Medium Duty Trucks	38	6	50	7	38	17	29	23		
Heavy Duty Tucks	0	8	0	10	83	41	64	44		
	Future Traffic (AM Peak)									
		M-	51			U	S-12	12		
	M-51 Nort	h of US-12	M-51 South of US-12		US-12 East of M-51		US-12 West of M-51			
	NB	SB	NB	SB	EB	WB	EB	WB		
Speed (mph) ¹	50	50	50	50	55	55	55	55		
Total	1093	949	1434	1013	853	598	950	856		
Auto and Light Trucks	1050	870	1377	994	716	495	798	708		
Medium Duty Trucks	43	70	57	8	43	31	48	45		
Heavy Duty Tucks	0	9	0	11	94	72	104	103		

^{1.} posted speeds or for Autos/Medium Trucks/ Heavy Trucks

Source: MDOT PEL Study

3.9 Existing Condition and Common Noise Environments

3.9.1 Existing Land Use and Zoning

Land uses within the Project study area are a mix of residential (single- and multi-family), commercial, industrial, and undeveloped land. Undeveloped areas are assumed to be available for future residential or commercial development.

3.9.2 Common Noise Environments

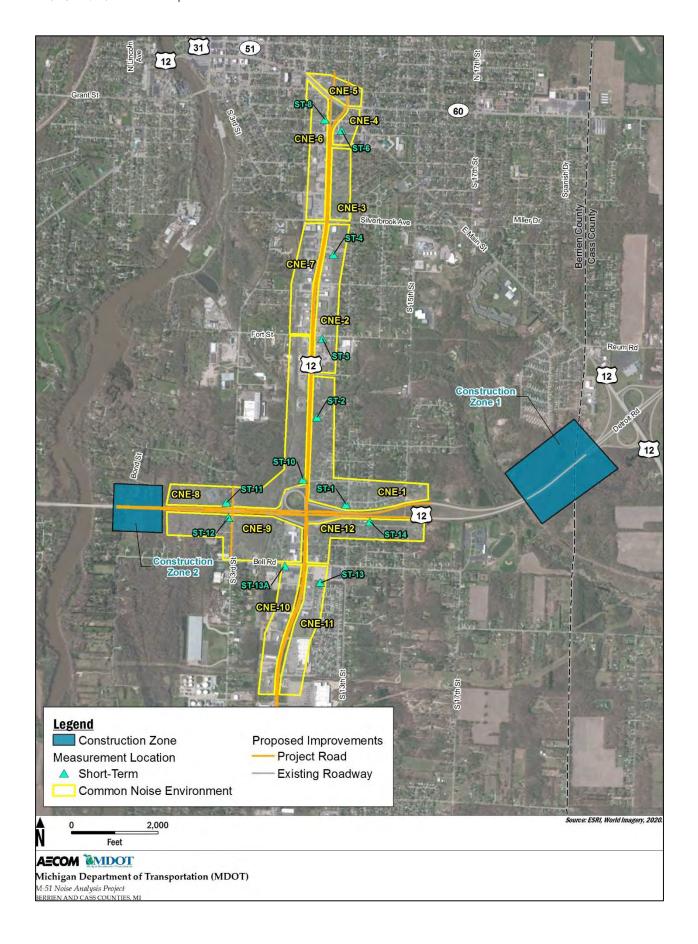
To better categorize the potential noise impacts and evaluate noise abatement for the various project alternatives, all of the potentially impacted noise-sensitive receptors have been organized into Common Noise Environments (CNEs). A CNE is defined as an area containing land uses that share a common highway traffic noise influence. Descriptions of delineated CNEs, including location, primary land use, and type of noise-sensitive receptors are listed in Table 3-2. Figure 3-2 shows an overview of the Project area illustrating the defined CNEs.

Table 3-2 Common Noise Environments

CNE	Location	Land Use	Measurement ID
CNE-1	North of US-12, East of M-51	Single Family Homes	ST-1, ST-2, ST-3
CNE-2	North of Brandywine St., East of M-51	Commercial, Single Family Homes	ST-4
CNE-3	North of Silverbrook St., East of M-51	Cemetery, Baseball Park	None*
CNE-4	North of Cherry St., East of M-51	Single Family Homes, Commercial	ST-6
CNE-5	North of Main	Single Family Homes	None*
CNE-6	North of Silverbrook St., West of M-51	Commercial, Single Family Homes	ST-8
CNE-7	North of Fort St., West of M-51	Commercial	None*
CNE-8	North of US-12, West of M-51	Commercial, Hotel Single Family Homes, Public Park	ST-10, ST-11
CNE-9	South of US-12, West of 3rd St.	Single Family Homes	ST-12
CNE-10	South of Bell St., West of M-51	Commercial, Hotel	ST-13A
CNE-11	South of Bell St., East of M-51	Commercial, Single Family Homes	ST-13
CNE-12	South of US-12, East of M-51	Single Family Homes	ST-14

^{*}Note: Noise measurements were unable to be performed at CNE-3, CNE-5, and CNE-7 due to inclement weather

Figure 3-1. Common Noise Environments and Noise Measurement Sites



3.9.3 Existing Noise Environment

3.9.3.1 Field Noise Measurements

Noise measurements were conducted for this project between September 20 and September 24, 2021. Noise measurements were conducted to provide information for noise model validation (short-term measurements with accompanying classified traffic counts) and to establish the loudest traffic noise hour. Noise measurements were conducted as described in Section 3.2. Appendix A includes measurement-related materials.

A total of twelve ST noise measurements were conducted as summarized in Table 3-3. Figure 3-2 contains an aerial figure of the Project area showing each measurement location.

3.9.3.2 Noise Model Validation and Results

The FHWA TNM Version 2.5 was used to predict noise levels for both the existing condition and future build alternative at receptor locations where noise levels are dominated by traffic noise on project roadways. To demonstrate that the noise model is predicting traffic noise levels within a reasonable margin of error, the noise model runs were validated by comparing predicted noise levels to measured noise levels for similar traffic conditions. However, since the TNM only predicts noise levels associated with traffic noise, the model runs can only be validated at measurement locations where noise levels were dominated by project roadways. For this project, noise model validation was possible for all twelve ST noise measurement locations. Noise models are considered to be validated if the difference between measured and modeled noise levels for comparable conditions is 3 dBA or less. The successful results of the noise validation effort are presented in Table 3-3.

Table 3-3 TNM Validation Summary

Measurement ID and Location	Obser	ved Traffic Co	unt	Measured Leq, dBA	Modeled Leq, dBA	Difference
	Туре	US-12 EB	US-12 WB			
	Autos	438	426			
ST-1	Medium Trucks	10	16			0.0
31-1	Heavy Trucks	46	62	58.7	57.8	-0.9
	Busses	0	0			
	Motorcycles	2	0			
	Туре	M-51 NB	M-51 SB			
	Autos	651	730			
ST-2	Medium Trucks	27	6	C2 F	CO 0	0.7
51-2	Heavy Trucks	0	8	63.5	62.8	-0.7
	Busses	3	4			
	Motorcycles	0	0			
	Туре	M-51 NB	M-51 SB			
	Autos	945	702	04.6		1.0
07.0	Medium Trucks	21	6		00.0	
ST-3	Heavy Trucks	3	9	61.6 62.6		1.0
	Busses	3	0			
	Motorcycles	0	3			
	Туре	M-51 NB	M-51 SB	- 57.9 57.8		
	Autos	945	702			
OT 4	Medium Trucks	21	6		57.0	
ST-4	Heavy Trucks	3	9		-0.1	
	Busses	3	0			
	Motorcycles	0	3			
	Туре	M-51 NB	M-51 SB		61.8	2.2
	Autos	495	380			
07.0	Medium Trucks	3	6	50.0		
ST-6	Heavy Trucks	12	0	59.6		
	Busses	6	0			
	Motorcycles	0	0			
	Туре	M-51 NB	M-51 SB			
	Autos	495	380			
07.0	Medium Trucks	3	6	20.7	20.4	
ST-8	Heavy Trucks	12	0	62.7	63.4	0.7
	Busses	6	0			
	Motorcycles	0	0			
	Type	M-51 NB	M-51 SB			
	Autos	651	730			
ST-10	Medium Trucks	27	6	67.6	69.0	1.4
	Heavy Trucks	0	8			
	Busses	3	4			1

Measurement ID and Location	Obser	ved Traffic Co	unt	Measured Leq, dBA	Modeled Leq, dBA	Difference
	Motorcycles	0	0			
	Туре	US-12 EB	US-12 WB			
	Autos	279	306			
ST-11	Medium Trucks	33	30	68.6 70.2	70.0	1.6
31-11	Heavy Trucks	48	45		70.2	1.6
	Busses	0	0			
	Motorcycles	0	0			
	Туре	US-12 EB	US-12 WB			
	Autos	279	306			
ST-12	Medium Trucks	33	30	68.9	68.9	0.0
31-12	Heavy Trucks	48	45	00.9	00.9	
	Busses	0	0			
	Motorcycles	0	0			
	Туре	M-51 NB	M-51 SB			
	Autos	543	756	52.9 54.2		
ST-13	Medium Trucks	21	36		F4.0	1.3
51-13	Heavy Trucks	3	12		1.3	
	Busses	3	0			
	Motorcycles	0	0			
	Туре	M-51 NB	M-51 SB			-0.1
	Autos	543	756			
ST-13A	Medium Trucks	21	36	60.2	60.1	
31-13A	Heavy Trucks	3	12	00.2	60.1	-0.1
	Busses	3	0			
	Motorcycles	0	0			
	Туре	US-12 EB	US-12 WB			
	Autos	438	426			
ST-14	Medium Trucks	10	16	69.7	67.6	-2.1
31-14	Heavy Trucks	46	62	09.1	07.0	-2.1
	Busses	0	0			
	Motorcycles	2	0			

As shown in Table 3-3, all calculated differences between modeled and measured noise levels are less than 3.0 dBA, therefore, the noise model predictions are considered to be valid.

TNM validation runs developed for this Project are digitally archived and will be made available upon request.

4. Noise Impact Analysis

4.1 Future Noise Levels and Impacts

This section presents predicted noise levels and noise impacts (or noise impact distances for identified CNE areas and general undeveloped areas).

4.1.1 Predicted Noise Levels and Noise Impacts

Traffic noise impacts, as defined in 23 CFR 772.5, occur when the design year condition noise levels approach or exceed the noise abatement criteria (NAC) specified in 23 CFR 772, or design year condition noise levels create a substantial noise increase over existing noise levels. 23 CFR 772 does not specifically define the terms "substantial increase" or "approach"; these criteria are defined in the MDOT Noise Analysis and Abatement Guidelines (July 13, 2011), as described in the following section. Table 2-3 summarizes the FHWA NAC corresponding to various defined land use activity categories.

MDOT noise handbook defines that a noise impact occurs when the sound level approaches or exceeds the NAC level, which is defined as an Leq(h) sound level 1 dBA less than the NAC identified in 23 CFR 772. This means that a loudest-hour noise level of 66 dBA is considered to approach the NAC for Category B of 67 dBA and is identified as an impact. The MDOT noise handbook defines a noise increase as substantial when the predicted traffic noise levels with project implementation exceed existing noise levels by 10 dBA. All conventional modeling techniques and recommendations for TNM by both FHWA and MDOT were implemented, as described in Section 3.7.

Table 4-1 below contains a summary of the predicted noise levels and noise impacts at all modeled CNE locations in the Project. Figures 5-1 (CNE-1), 5-2 (CNE-2 and CNE-7), 5-3 (CNE-3, CNE-4, CNE-5, and CNE-6), 5-4 (CNE-8), 5-5 (CNE-9), 5-6 (CNE-10 and CNE-11), and 5-7 (CNE-12) contain detailed aerial imagery of the Project area showing all modeled receptor locations and predicted future build impacts. Due to the large number of modeled receptors and CNEs within the Project area, prediction information for individual receptors is presented in detail in Appendix C.

Table 4-1 Summary of Predicted Noise Levels by CNE

ONE	No. of	Total		Predicted Noise Level (Range), Leq (1h)		Total Number of Noise Impacted Units		
CNE	Modeled Receptors	Dwelling Units	Existing	Future Build	Approach or Exceed NAC	Significant Increase	Total Impacted DU	
CNE-1	56	56	52.8 - 65.7	53.5 - 68.8	9	0	9	
CNE-2	12	16	51.8 - 67.4	52.4 - 68.0	0	0	0	
CNE-3	10	8	56.8 - 61.4	57.4 - 61.9	8	0	8	
CNE-4	19	20	55.5 - 71.5	55.9 - 71.8	6	0	7	
CNE-5	26	26	46.0 – 70.0	46.2 - 70.1	4	0	4	
CNE-6	52	52	49.9 - 64.5	50.4 - 64.9	0	0	0	
CNE-7	1	0	66.0	68.7	0	0	0	
CNE-8	7	4	57.7 - 65.8	59.2 - 66.5	1	0	1	
CNE-9	14	14	55.6 - 67.5	56.1 - 68.5	3	0	3	
CNE-10	0	0	NA	NA	0	0	0	
CNE-11	12	12	52.6 - 56.6	53.2 - 57.2	0	0	0	
CNE-12	32	32	53.7 - 68.9	53.9 - 71.2	6	0	6	

Figures showing all receiver locations along with evaluated noise abatement elements are included in Section 5.

5. Noise Abatement Evaluation

5.1 Noise Abatement Measures

According to FHWA and MDOT policies, when noise impacts are identified, noise barriers (at a minimum) must be considered as noise abatement. Other potential noise abatement measures might include heavy truck or speed restrictions, alignment changes, and depressed roadways. Of these alternatives, the Project alignment was evaluated and compared for noise impacts (as presented in Section 4), but truck restrictions and speed restrictions below proposed speed limits would significantly reduce the value of the roadway. Noise barriers were evaluated for each CNE with noise impacts for feasibility and reasonableness. The following section describes the results of the barrier assessments for each evaluated CNE.

5.2 Feasible and Reasonable Criteria and Requirements

For abatement to be recommended, the barrier must meet certain feasibility and reasonableness requirements established by MDOT in the Noise Analysis and Abatement Guidelines.

When noise barriers are considered, a preliminary noise barrier design analysis must show that the barrier is feasible. According to the MDOT noise handbook, feasible noise barriers must provide at least 5 dBA of noise reduction to 75% of the impacted receptors. In addition to meeting minimum noise reduction requirements, noise barriers must also meet engineering and constructability feasibility requirements in terms of safety, property and emergency access, drainage control, overhead and underground utility clearance, and other issues.

Noise barrier reasonableness is generally related to cost-effectiveness and benefited receptors, where a benefited receptor receives at least 5 dBA of noise reduction (NR), and cost-effectiveness is driven by a Cost per Benefited Receptor Unit (CPBU) value. The handbook identifies a CPBU of \$49,301, which is a final quotient resulting from dividing the total cost of abatement (at a rate of \$45.00 ft²) by the total number of benefited receptors. Additionally, The MDOT design year attenuation requirement requires that a minimum of one benefited receptor achieve at least a 10 dBA noise reduction and that at least 50% of benefited receptors achieve a 7dBA reduction for noise abatement to be reasonable.

To summarize, for a barrier to be considered feasible and reasonable, it must have:

- A noise reduction of at least 5 dBA must be achieved at 75% of impacted receptors
- A noise reduction of 10 dBA must be achieved for at least one receptor
- A noise reduction of 7 dBA must be achieved at 50% of benefitted receptors

For a noise barrier to be considered reasonable in addition to the requirements listed above, the viewpoints of benefited property owners and residents must be taken into consideration. Greater than 50% in favor of all responding benefited owners and residents is needed to construct noise abatement. Public viewpoints and votes of benefited receptors are not part of this noise analysis but are collected during the Preliminary Engineering Phase and are recorded in the environmental documentation.

5.3 Findings and Recommendations for Noise Abatement

Noise abatement was considered for each CNE with identified noise impacts. Initially, noise abatement was checked for feasibility (5 dBA reduction for at least 75% of impacted receptors and access restrictions). If abatement was determined to be feasible, the abatement was analyzed for cost-effectiveness and other reasonableness factors. For all impacted receptors meeting feasibility requirements, preliminary barrier designs were evaluated using TNM. If the abatement was found to be both reasonable and feasible, it would be recommended for inclusion in the project pending a polling of viewpoints from benefited receptors. A summary of the barrier locations and resulting sound levels are provided in Table 5-1. The details of the barrier analysis including determinations of feasibility and reasonableness are included in Table 5-2. The narrative results of abatement evaluations for each impacted CNE are summarized in subsequent sub-sections.

Table D-1 in Appendix D lists the predicted existing, future build, and future build with barrier noise levels per modeled receptor location. The table also includes the information regarding benefited receptors and barrier design goal achievement.

Table 5-1 Evaluated Barrier Descriptions

Barrier ID	Location	Existing Leq (dBA)	Future Leq I	Range (dBA)	Barrier Noise Reduction	Barrier Geometries (feet)	
			No Barrier	With Barrier	(dBA)	Length	Avg. Height
Wall 1A	CNE 1, along US12 ROW, east of M51 intersection	61-66	63-69	57-62	1-10	1400	11.5
Wall 1B	CNE 1, along M51 ROW, north of Oakdale, along proposed sidewalk	56-66	56-66	54-62	1-7	400	15.75
Wall 3	Along M51, Following fence line of existing cemetery	68-69	69-70	60-64	5-10	1100	6.36
Wall 4	CNE 4, along M51, south of Main St, between existing sidewalk and ROW line	60-70	60-71	58-61	3-12	250	9.2
Wall 5	Along M51, South of Main St, between existing sidewalk and ROW line	60-71	66-69	59-62	5-10	200	9.5
Wall 12	CNE 12, along US12 ROW, east of M51 intersection	54-68	55-71	53-66	0-10	600	9.5

Table 5-2 Barrier Analysis Results

Barrier ID	Number of Attenuated Locations ¹									
	≥ 10 dBA	≥ 7 dBA		≥ 5 dBA (Benefitted Receptors)		Cost ²	Cost Per Benefitted	Feasible?	Reasonable?	Recommended?
		#	% of Benefit	#	% of Impacts		Unit			
Wall 1A	3	6	67%	9	100%	\$724,500	\$80,500	Yes	No	No
Wall 1B	0	1	100%	1	100%	\$283,500	\$283,500	Yes	No	No
Wall 3	1	6	75%	8	100%	\$314,820	\$39,353	No	Yes	No
Wall 4	2	3	75%	5	100%	\$103,500	\$20,700	No	Yes	No
Wall 5	1	1	50%	2	100%	\$85,500	\$42,750	No	Yes	No
Wall 12	1	1	50%	2	67%	\$256,500	\$128,250	No	No	No

Note:

1) MDOT policy requires that reasonable and feasible noise walls must be constructable, provide at least 10 dBA noise reduction at one impacted receptor, at least 7 dBA noise reduction for at least 50% of benefited receptors, at least 5 dBA noise reduction for at least 75% of impacted receptors, and be constructed at an estimated cost of no more than \$49,301 per benefited receptor.

2) Wall costs reported here are based on wall area in square feet as calculated by TNM times MDOT unit cost of \$45.00/square foot.

5.3.1 CNE-1 Noise Abatement Analysis

CNE-1, north of US-12 and east of M-51, contains 56 modeled receiver locations representing a total of 56 individual single-family homes with each home representing one dwelling unit. Nine receptors were determined to be impacted under the future build condition. Two noise walls were analyzed, Wall 1A on the north side of US-12, and Wall 1B on the east side of M-51. Neither wall was found to meet MDOT reasonableness standards. Wall 1A would cost at least \$80,500 per benefitted receptor, exceeding the allowable CPBU. Wall 1B also exceeded the CPBU and did not achieve a 10 dB reduction at an impacted receptor. Thus, abatement is not recommended for this CNE. These walls are shown in Figure 5-1.

5.3.2 CNE-2 Noise Abatement Analysis

CNE-2 contains 12 modeled receiver locations representing a total of 16 individual dwelling units, none of which were impacted. As there were no impacts, no abatement was analyzed. CNE-2 is shown in Figure 5-2.

5.3.3 CNE-3 Noise Abatement Analysis

CNE-3 contains two separate land uses, a cemetery, and a public baseball field, both of which would be considered an Activity Category C land use with an exterior impact threshold of 66 dBA, Leq. The baseball field, Thomas Memorial Stadium, was determined not to be impacted due to a 40-foot set back from M-51 and noise reduction provided by an existing solid 8-foot-high wall surrounding the playing field and seating area. However, the cemetery, city owned Silverbrook Cemetery, has no such acoustical protection. Guidance in Appendix D of the MDOT Highway Noise Analysis and Abatement Handbook was used to determine Dwelling Unit Equivalents (DUEs) for the cemetery. The cemetery contains about 77,000 square feet of land within the 66 dBA noise impact distance from M-51, extending about 70 feet in from the cemetery fence line. When compared to a typical lot size of a nearby home (821 S. 15th St. - 9,652 square feet) this equates to 8 impacted DUEs. A noise wall 1100 feet long and with an average height of 6.4 feet at this location would have met MDOT requirements for acoustical performance and cost. However, there are several considerations that would create feasibility issues for a wall at this location. First, the cemetery has been identified as an historic property so the existing iron fence would probably need to remain, and a noise wall located further to the west, which may also require relocating the sidewalk at substantial additional cost. Second, the only available wall alignment coincides with overhead power lines and an underground gas line that would impact constructability. Finally, it was judged that this historic part of the cemetery is very lightly used, with new burials occurring in this section only once or twice a year and very few visitors according to cemetery staff, so the benefit of a noise wall at this location would be very limited. Therefore, a noise wall is not recommended for this location. CNE-3 is shown in Figure 5-3.

5.3.4 CNE-4 Noise Abatement Analysis

CNE-4 is east of the northernmost stretch of M-51 within the project area and contains 19 modeled receptor locations representing 20 individual dwelling units, primarily single-family homes and one multi-family residence. Seven dwelling units were determined to be impacted under the future build condition. Wall 4 was analyzed along M-51, extending 250 feet from north of Hickory Street to Oak Street/M-60BR between the existing sidewalk and ROW line. The noise wall at this location was ultimately determined to be not feasible in accordance with MDOT noise policy for several reasons. These included significant constructability issues associated with interference with existing drainage features, utility conflicts (overhead electric, underground gas, watermain, fiber optic and telephone), conflicts with adjacent existing sidewalk as well as sidewalk connectivity to E. Main Street. In addition, a clear safe zone in this area would require a noise wall to be located 16 to 18 feet from the near travel lane which would be in very close proximity to existing residential structures. For these reasons, a noise wall is not recommended for this area. CNE-4 is shown in Figure 5-3.

5.3.5 CNE-5 Noise Abatement Analysis

CNE-5 contains 26 modeled receptors representing a total of 26 dwelling units, all single-family homes. Four receptors were determined to be impacted under future build conditions. Two impacted receptors are located on Oak Street at the southern end of the CNE. Abatement for these receptors would block street access, therefore, no abatement was analyzed. The other two impacted receptors, 05-06 and 05-07 are located alongside Main Street at the northwestern corner of the CNE north of E. Main Street between Cedar Street and N. 10th Street. A 200-foot-long, 10-foot-high wall along Main Street could provide the required noise reduction for the two impacted receptors. However, a noise wall constructed at a sufficient setback distance to provide a safe clear zone from traffic on Main Street (approximately 18 feet) would be located just a few feet from the corner of the house represented at 05-07 (914 Cedar Street), creating safety and constructability issues. It is also noted that the proximity of the wall to the south-west corner of the house at this location would restrict or eliminate access to the back yard area from the house and may also create potential damage issues to the foundation of the structure. Therefore, noise abatement at this location is considered to be not feasible and is not recommended. CNE-5 is shown in Figure 5-3.

5.3.6 CNE-6 Noise Abatement Analysis

CNE-6 contains 52 modeled receptor locations representing 52 dwelling units, none of which were impacted. As there were no impacts, no abatement was analyzed. CNE-6 is shown in Figure 5-3.

5.3.7 CNE-7 Noise Abatement Analysis

CNE-7 contains one modeled receptor location, a single restaurant with an outdoor eating area. This receptor was determined not to be impacted by future build conditions; therefore, no abatement was analyzed. CNE-7 is shown in Figure 5-2.

5.3.8 CNE-8 Noise Abatement Analysis

CNE-8 contains seven modeled receptor locations representing a total of four individual dwelling units, one of which was impacted. Following a basic assumption that a barrier would need to extend at least 3 times the distance from the barrier to the receiver in each direction and be tall enough to block the line of sight to the highway vehicles, a barrier of at least 800 feet in length and at least 12 feet in height would be needed to provide a minimum of 5 dBA reduction at the receptor. At \$45/square foot, this barrier would cost at least \$432,000 per benefitted receptor, far exceeding the CPBU. Thus, no abatement was modeled for this location. CNE-8 is shown in Figure 5-4.

5.3.9 CNE-9 Noise Abatement Analysis

CNE-9 contains 14 modeled receptor locations representing a total of 14 individual dwelling units, of which three were impacted. Impacted receptors included two single-family homes located along 3rd Street, represented by receptors 09-07 and 09-09, and another single-family home southwest of the intersection, represented by receptor 09-01. Noise impacts at the receptors along 3rd Street (09-07 and 09-09) were determined to be in part due to traffic on 3rd Street, which cannot be mitigated for without cutting off street access to these homes, therefore any abatement for noise from US12 would not adequately reduce noise levels at the impacted receptors. Therefore, no abatement was analyzed for this location. CNE-9 is shown in Figure 5-5.

5.3.10 CNE-10 Noise Abatement Analysis

CNE-10 contains no noise-sensitive land uses; thus no abatement was analyzed. CNE-10 is shown in Figure 5-6.

5.3.11 CNE-11 Noise Abatement Analysis

CNE-11 contains 12 modeled receptor locations representing 12 dwelling units, all single-family homes, none of which were impacted. As there were no impacts, no abatement was analyzed for this area. CNE-11 is shown in Figure 5-6.

5.3.12 CNE-12 Noise Abatement Analysis

CNE-12, located south of US-12 and east of M-51, contains 32 modeled receptor locations representing 32 dwelling units, of which six were impacted. The receptors in this area consist solely of single-family homes. Three of the impacted receptors are located along M-51, with direct driveway access onto and intersecting with roads precluding abatement in this area, thus no abatement was considered for these receptor locations. The remaining three receptors are located along US-12; two are within 200 feet of each other (12-05 and 12-06) and the third is approximately 1,100 feet further to the east (12-21). Following the same assumptions used for CNE-8, it was determined that a barrier at least 320 feet in length and 8 feet in height would be required to provide 5 dBA of noise reduction for the individual receptor location (12-21), costing \$115,200 and exceeding the maximum allowable CPBU value. Therefore, no noise abatement was considered for this receptors location. For the other two locations (12-05 and 12-06), a wall 600 feet in length with an average height of 9.5 feet could provide benefit to both impacted receptors, including a 10 dBA reduction at a single impacted receptor, but was otherwise unable to meet MDOT reasonableness requirements due to a CPBU of at least \$128,250. Thus, this barrier is not recommended. CNE-12 is shown in Figure 5-7.

Figure 5-1 Acoustical Analysis for CNE-1



Figure 5-2 Acoustical Analysis for CNE-2 and CNE-7

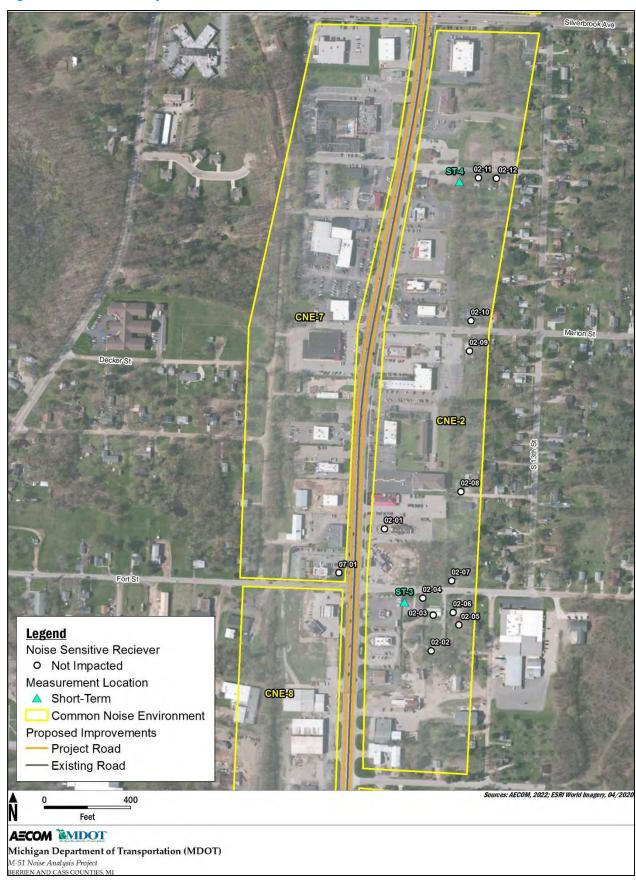


Figure 5-3 Acoustical Analysis for CNE-3, CNE-4, CNE-5, & CNE-6

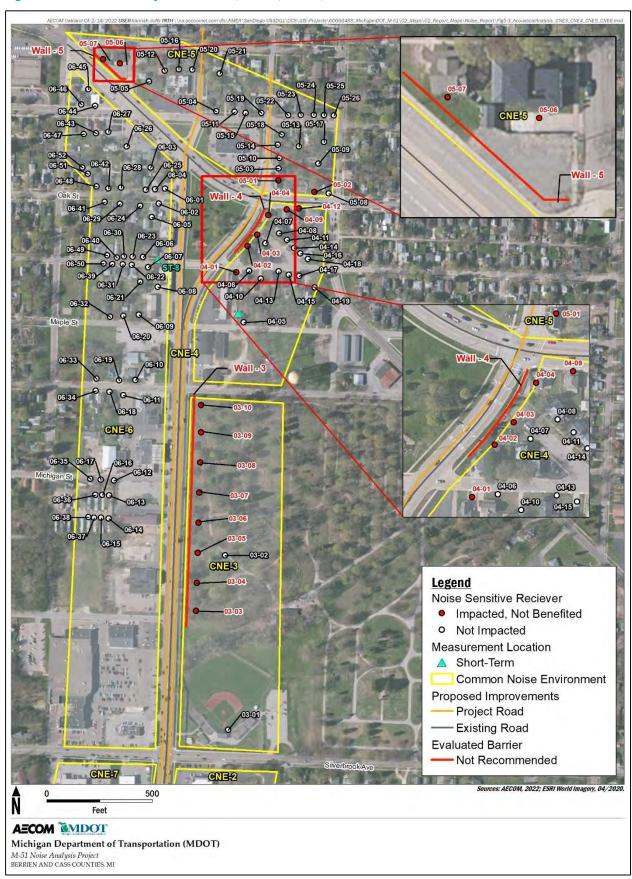


Figure 5-4 Acoustical Analysis for CNE-8



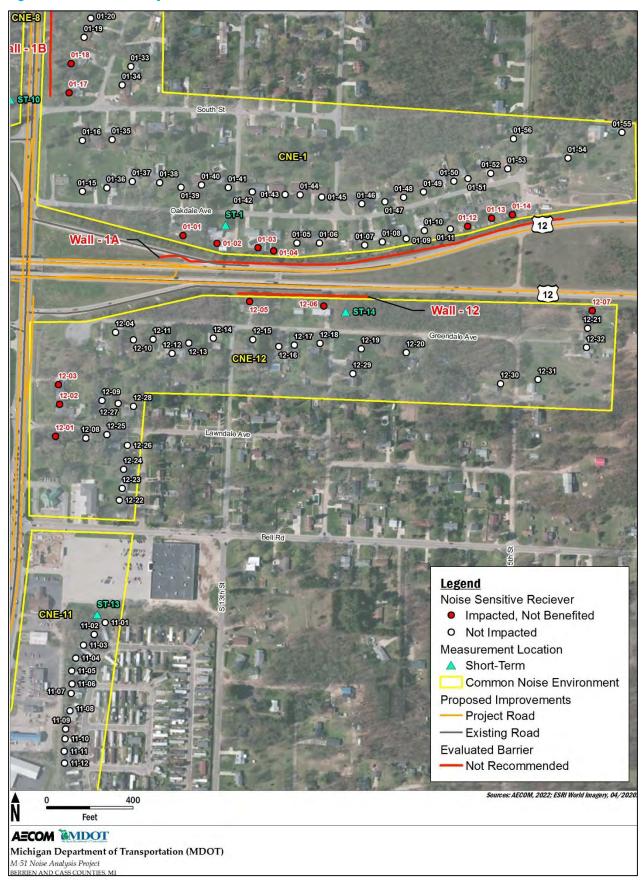
Figure 5-5 Acoustical Analysis for CNE-9



Figure 5-6 Acoustical Analysis for CNE-10 & CNE-11



Figure 5-7 Acoustical Analysis for CNE-12



6. Construction Noise Analysis

FHWA policy requires that construction noise be considered in a Type 1 highway noise analysis. This analysis would generally include the following:

- 1. Identification of land uses that may be affected by construction noise,
- 2. Determination of the measures needed in the plans and specifications to minimize or eliminate construction noise impacts; and,
- 3. Incorporate needed abatement into the plans and specifications.

Neither FHWA nor MDOT identify specific construction noise impact criteria. In addition, the detailed information necessary to predict actual construction noise levels (construction schedules, phasing, equipment lists, laydown areas, etc.) has not yet been determined. However, for this project, it is anticipated that pile driving and some nighttime construction work will be required.

It is recognized that areas adjacent to the highway right of way and other construction areas (such as staging areas and laydown sites) can temporarily be exposed to high levels of noise during peak construction periods. It is reasonable to assume that the same CNEs identified for potential traffic noise impacts could also be exposed to construction noise. The effect of the noise on the local area can be reduced if the hours and days of construction activity are limited to less sensitive time periods. The project construction standard noise specifications help minimize the effects of construction noise.

The following special provisions may be incorporated into the construction contract:

- Inform the local public in advance of construction activities that may generate particularly high noise levels (such as pile drivers) or periods of nighttime construction activity.
- Noise barriers approved for incorporation into the project should be constructed as close to the beginning of the project's construction timeline as practical.
- Noise created by truck movement shall not exceed 88 dBA at a distance of 50 feet.
- When working between 7:00 P.M. and 10:00 P.M., use "smart alarms" instead of standard reverse signal alarms or use spotters. When working between 10:00 P.M. and 7:00 A.M. use spotters instead of auditory alarms.
- Have portable noise meters on the job at all times for noise level spot checks on specific operations. Employ an individual trained in the use of noise meters, with working knowledge of sound measurements and their meaning and use as applied to these abatement/abatement measures.

6.1 Typical Construction Noise Levels

Table 6-1 contains a list of commonly used construction equipment and noise levels associated with using that equipment.

Table 6-1 Typical Construction Equipment Noise Levels

Equivalent Type	Lmax Ref dBA (50 feet)	AUF %
Auger Drill	84	20
Backhoe	78	40
Boring Jack Power Unit	83	50
Chain Saw	84	20
Compactor (ground)	83	20
Compressor (air)	78	40
Concrete Mixer Truck	79	40
Concrete Pump Truck	81	20
Concrete Saw	90	20
Crane	81	16
Dozer	82	40
Drill Rig Truck	79	20
Drum Mixer	80	50
Dump Truck	76	40
Excavator	81	40
Flat Bed Truck	74	40
Front End Loader	79	40
Generator (>25KVA)	81	50
Generator (<25KVA)	73	50
Gradall	83	40
Grader	85	40
Horizontal Boring Jack	82	25
Hoe Ram	90	20
Jackhammer	89	20
Man Lift	75	20
Pavement Scarafier	90	20
Paver	77	50
Pickup Truck	75	40
Pneumatic Tools	85	50
Pumps	81	50
Roller	80	20
Scraper	84	40
Shears (on backhoe)	96	40
Tractor	84	40
Vacuum Excavator	85	40
Vacuum Street Sweeper	82	10
Ventilating Fan	79	100
Vibrating Hopper	87	50
Vibratory Concrete Mixer	80	20
Warning Horn	83	5
Welder/Torch	74	40

Source: RCNM User Guide, Table 1 (actual measured Lmax)

6.2 Construction Noise Abatement Measures

Although MDOT does not identify any specific abatement measures related to construction noise, the following list could be considered best practices for the avoidance of any potential problems related to construction noise impacts:

- No construction shall be performed within 1,000 feet of an occupied dwelling unit on Sundays, legal holidays, or between the hours of 10 p.m. and 6 a.m. on other days without the approval of the MDOT construction project manager.
- All equipment used shall have sound-control devices no less effective than those provided on the original equipment. No equipment shall have unmuffled exhaust.
- All equipment shall comply with pertinent equipment noise standards of the U.S. Environmental Protection Agency.

- No pile driving or blasting operations shall be performed within 3,000 feet of an occupied dwelling unit on Sundays, legal holidays, or between the hours of 8 p.m. and 8 a.m. on other days without the approval of the MDOT construction project manager.
- The noise from rock crushing or screening operations performed within 3,000 feet of any occupied dwelling shall be mitigated by strategic placement of material stockpiles between the operation and the affected dwelling or by other means approved by the MDOT construction project manager.

If a specific noise impact complaint is received during construction of the project, the contractor may be required to implement one or more of the following noise abatement measures at the contractor's expense, as directed by the construction project manager:

- Locate stationary construction equipment as far from nearby noise-sensitive properties as feasible.
- Shut off idling equipment.
- Reschedule construction operations to avoid periods of noise annoyance identified in the complaint.
- Notify nearby residents whenever extremely noisy work will be occurring.
- Install temporary or portable acoustic barriers around stationary construction noise sources.
- Operate electrically powered equipment using line voltage power or solar power.

Special Construction Zones

In addition to construction noise associated with the proposed improvements within the defined project area, there are two defined "Construction Zones" on either end of the project area along US-12 (as shown in Figure 1-1). The purpose of these construction zones is to stage and construct a set of temporary cross-over ramps on either side of the project to redirect traffic on US-12 during the intersection reconstruction. Construction Zone 1, east of the project area, would be situated within approximately 300 feet of the Silverbrook mobile home community northwest of the US-12/E Main Street interchange. Construction Zone 2, west of the project, would be immediately adjacent to the Griffin Estates apartment complex northeast of the US-12/Bond Street intersection. Both Construction Zones would be close enough to temporarily create elevated noise levels at the nearby residential communities (depending on the type of equipment being used). It is therefore recommended to follow the same abatement measures listed above for construction activity within the vicinity of residential areas within the project.

7. Information for Local Government Officials

FHWA and MDOT policy specify that local officials should be provided appropriate information to assist with future compatible land use planning, especially regarding the planning and development of undeveloped lands near the proposed project right-of-way.

Table 7-1 shows noise impact distance for the 66 dBA and 71 dBA levels (NAC categories B/C and E, respectively) from both highways in the project area. Future developments should not place applicable noise-sensitive land uses within the distances listed from edge of pavement.

Table 7-1 Noise Impact Distances for Undeveloped Lands

	Distance From the Edge of Pavement (Feet)				
Project Roadway	71 dBA	66 dBA			
M-51	29	108			
US-12	54	136			

8. Conclusions and Recommendations

The noise analysis for the proposed project included a total of twelve measurement locations and 233 predicted representative noise levels for 232 dwelling units in the project area. The project was split into twelve separate CNEs for noise impact analysis within the study area.

Seven of the twelve CNEs contained receptors with predicted future noise levels approaching or exceeding the NAC. Noise abatement was evaluated in five locations. But none were found to be feasible and reasonable as defined by MDOT policy. Therefore, no noise abatement is recommended for this project.

9. Statement of Likelihood

Based on the studies thus far accomplished, MDOT does not intend to install highway traffic noise abatement for this project. The preliminary noise abatement measures were based on preliminary roadway design, and design and costs for noise abatement as presented in Table 5-2 in this document. If roadway designs have substantially changed during the final design process, noise abatement measures may be re-evaluated.

10. References

Federal Highway Administration, 23 CFR 772, Procedures for Abatement of Highway Traffic Noise and Construction Noise, July 2010. https://www.fhwa.dot.gov/legsregs/directives/fapg/cfr0772.htm

Federal Highway Administration (FHWA). 2011. Highway Traffic Noise: Analysis and Abatement Guidance. U.S. Department of Transportation, Federal Highway Administration, Washington, DC. .

https://www.fhwa.dot.gov/environment/noise/regulations and guidance/analysis and abatement guidance/revguidance.pdf

Michigan Department of Transportation, Highway Noise Analysis and Abatement Handbook. July 13, 2011. https://www.michigan.gov/documents/mdot/MDOT HighwayNoiseAnalysis and AbatementHandbook 358156 7.pdf

Appendix A Noise Measurement Data and Documentation

Appendix A contains the following noise measurement data and documentation:

- Short-term Noise Measurement Summary Table
- Noise Measurement Photo Log
- Noise Measurement Field Data Sheets
- Noise Measurement Equipment Calibration Certificates

Short Term Measurement Summary

ID	Location	Average Leq (dBA)	Leq Range (dBA)	Start (hh:mm)	Stop (hh:mm)	Duration (hh:mm)
ST-1	1228 Oakdale Ave	58.7	54-62.1	11:24	11:39	0:16
ST-2	1103 North St	63.5	61.8-66	11:08	11:40	0:33
ST-3	1401 S 11th St	61.6	56.2-65.6	14:22	14:51	0:30
ST-4	1001 S 11th St	57.9	54.8-63.3	14:22	14:53	0:32
ST-6	1119 Maple St	59.6	54.1-66.9	13:17	13:50	0:33
ST-8	939 Hickory St	62.7	59.2-66.7	13:20	13:48	0:27
ST-10	1556 S 11th St	67.6	65-70.4	11:10	11:39	0:30
ST-11	1730 S 3rd St	68.6	64.1-72.3	9:30	9:50	0:21
ST-12	1814 S 3rd St	68.9	64.7-71.1	11:16	11:38	0:23
ST-13	1908 S 11th St	52.9	50-56.2	12:03	12:26	0:24
ST-13A	1016 Bell Rd	60.2	55.5-68.8	12:05	12:28	0:24
ST-14	1325 Greendale Ave	69.7	64-74.2	9:28	9:51	0:23

Noise Measurement Photo Log

ST-01 1228 Oakdale Ave.



ST-02 North Street



ST-03 1124 Fort Street



ST-04 1122 Lambert Street



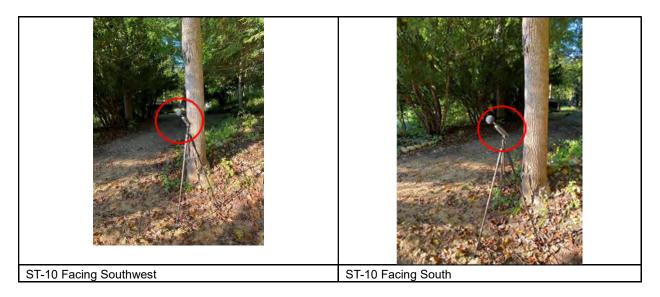
ST-06 1119 Maple Street



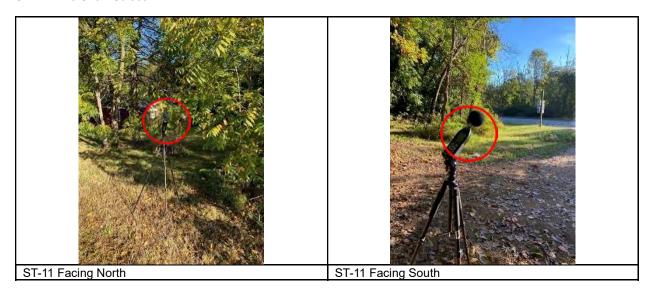
ST-08 939 Hickory Street



ST-10 1556S. 11th Street /M-51



ST-11 1776 S. 3rd Street



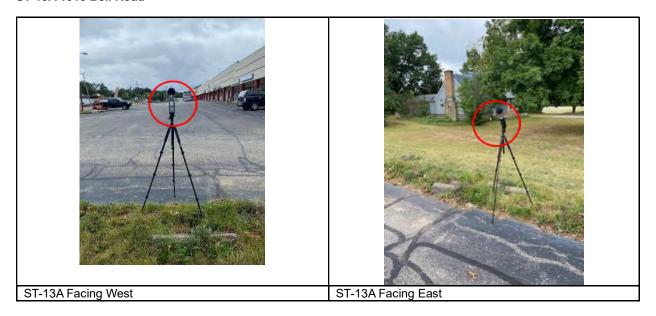
ST-12 1814 S. 3rd Street



ST-13 Big Lots Parking Lot



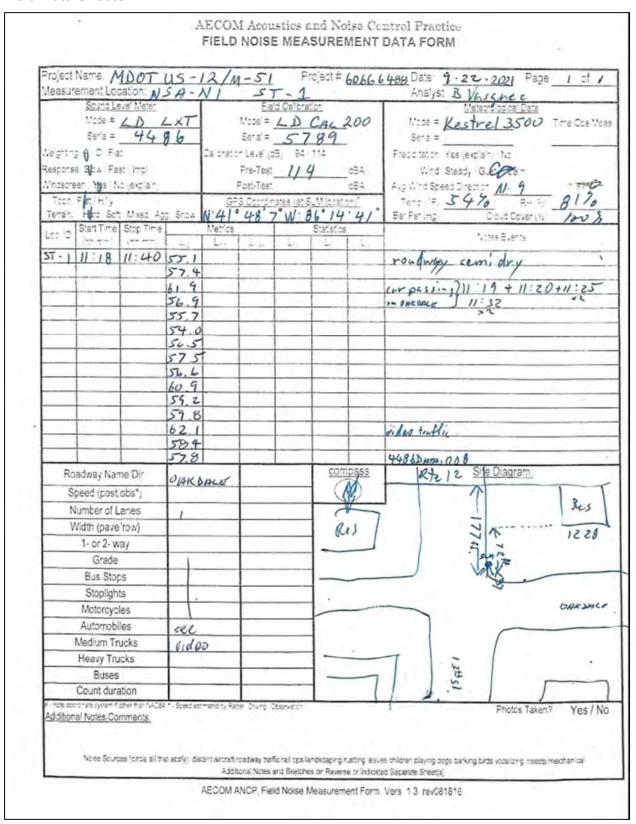
ST-13A 1016 Bell Road



ST-14 Greendale Ave.



Field Data Sheets



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AECOM Acoustics and Noise Control Practice FIELD NOISE MEASUREMENT DATA FORM US-12/M-51 Project Name: MDoT Project #. 606664 88 Date: 9/20/21 Page / of / Measurement Location: 5T-L Analyst: 64 Sound Level Meter Field Calibration Model #: LD LXT Model #: KeStrel 3500 Time Obs/Meas Model #; Serial #: 4926 Serial #: 2058303 14:22 Serial #: Weighting A C / Flat Precipitation: Yes (explain) (No) Calibration Level (dB): 94 / 114 Response: (Slow) Fast / Impl Wind: Steady / Gusty / Calm Pre-Test Avg Wind Speed/Direction: 1—2 N, m/s (MPH) Temp (°F): 29 81-1 RH (%): 68-4 Bar Psr (Hg): 29.22 Cloud Cover (%): 60-4 Windscreen (Yes) No (explain) Post-Test Topo:(Flat)/ Hilly GPS Coordinates (at SLM location)" Terrain: Hard / Soft (Mixed) Agg / Snow 41.8176923, -86,2464 379 Start Time Stop Time Statistics Metrics Notes/Events (hh:mm) (hh:mm) L50 14:24 14:58 Buntimen Mexet time off by -3 min. 55.4 56.8 14:30 14:35 55.6 56.6 14:40 56.3 58.6 14:45 14:50 14:55 56.8 Site Diagram: compass Roadway Name/Dir. M-51 Speed (post/obs*) 50 mph 4 Number of Lanes Width (pave/row) 1- or 2- way Grade Bus Stops SLM Stoplights 'n 2201 Lambert Motorcycles Ž Automobiles 549 Medium Trucks 9 Heavy Trucks 4 Buses 20 mln. Count duration Photos Taken? Audible Additional Notes/Comments: Distant Landscaping Noise Sources (circle all that apply): distant aircraft codway trafficial opsilandscaping/rustling teaves children playing/dogs barking/birds vocalizing/insocsylmechanical Additional Notes and Sketches on Reverse or Indicated Separate Sheet(s) File.007 AECOM ANCP, Field Noise Measurement Form, Vers. 1.3 rev081816

AECOM Acoustics and Noise Control Practice FIELD NOISE MEASUREMENT DATA FORM Project Name: MDOT U5-12/M-51 Project #: 60666U98Date: 9/22/21 Measurement Location: Analyst: 6 F1 Sound Level Meter Field Calibration Meteorological Data Model # LD CxT Model #: Kestrel 3500 Time Obs/Meas: Model #: CAL 200 Serial # 41926 Serial #: 6637 Serial #: 2058303 Weighting A/C/Flat Calibration Level (dB): 94 /(114) Precipitation: Yes (explain) / No Pre-Test -0.03 Response: (Slow) / Fast / Impl Wind: Steady / Gusty / Calm Post-Test + 0.03 dBA Windscreen : (Yes) No (explain) m/s (MPH) Avg Wind Speed/Direction: 1, 5 E Temp (*F):60.4/ Topo: (Flat) Hilly GPS Coordinates (at SLM location)" 411. 8252602, -86,2461030 Terrain: Hard / Soft (Mixed) Agg / Snow Bar Psr (Hg): 29, 23 Cloud Cover (%): Loc. ID Start Time Stop Time Metrics Statistics Notes/Events (hh:mm) (hh:mm) Leg Lone Lmax L10 L50 13:16 13:51 Bustime 13:41 Small Child on bike + Parent Passed by SLM, approx 3++ 13:48 Child + Parent returned, dog inside residence 3 houses down audible barking 13:20 55.4 13:25 54.8 13:30 63.3 13:35 58.7 13:40 46.3 13:45 58.3 13:50 59.0 compass Site Diagram: Roadway Name/Dir. M-51 SFR (1) Speed (post/obs*) 50 Number of Lanes 41 Width (pave/row) 1- or 2- way 2 Grade Maple S Bus Stops NB 2 Stoplights Indust born Motorcycles Automobiles 165 Medium Trucks Heavy Trucks 4 Buses 2 Count duration 20 min. note coordinate system if other than NADBA Photos Taken? (Yes/No Additional Notes/Comments: Noise Sources (circle all that apply): distant siroral roadway traffigliari operandscaping questing leaves children playing/dogs barking/birds vocalizing/insects/hechanical Additional Notes and Sketches on Reverse or Indicated Separate Sheet(s) AECOM ANCP, Field Noise Measurement Form, Vers. 1.3 rev081816

Project Name: MDOT Measurement Location: N	US-12/M-	51 Pr	oject# 6066 6	6488 Date: 9.22.2021 Page 1.df Analyst B Vasquez
Sound Leve' Meter	SHIND ST.	Field Calibrat	ion	Meteor Cooka Data
Mode = AD			CAL 200	Vista = Kestrel 3500 Traces.
Seria = 44		18= 57		Sera R
Neighting & C. Flat		eve (d3) 94		Préopitation Yes (exglein) Q
Response St A Fast Imp		e-Test /14		Wind Steady Gus 2-
Aindscreen : Yes / No (explain		t-Test	d8A	Aug Wind Speed Director 10 M - stk
Topo Flet/Hily		cordinates lat 8	Mildeaton*	Ter: F 55° RH 7676
Terrain: Hard Soft Mixed	ADD STON N' 410 4	9'34WB	6'14'50"	Bat Far (Hg) Cloud Cover (%) 100
Start Time Stop Tim	re Metrics		Statistics	Notes Events
The American	The Late of the	La L	The Land	1.7/5 E.fo 'S
ST. 8 13:20 13:5				
	59.2			13:31 siren NB m51
	62.8			13:36 garbage Inch on Hake
	63.9		-	13:40 train hern
	63.2			13. TO Train Wen
	63.2			
	61.5			
	60.5			
	60.3			
	63.7			
	69.7	-		-
	61.1			
	60.6			44860000000
Roadway Name Dir			compass	Site Diadram:
Speed (postlobs*)	M 51		(A)	
Number of Lanes	1 0		W	
	2		-	M-51
Width (pave row)				M-)
1- or 2- way	CIVEL			
Grade	-		ł	
Bus Stops	~			Store
Stoplights	1		1	
Motorcycles			1	
Automobiles	190		1	+
Medium Trucks	3			7 ASLAN ES
Heavy Trucks			-	7 4 \$
Buses			Res	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
Count duration	130 min		939	
 tale pording system faces for VA Additional Notes Comments. 	Tex sceed assumed by 430%			Photos Taken? Yes /
Additional Notes Collins	EMT siren			
Notes Solmes (rimis at	that apply distant amount for	and and are to	Acres on married	es children playing dags carking birds vocalizing insects meditah cal

Project Name: MDOT	US-12/M-5	1 Project # 6066	6488 Date 9 2 1 2021 Page 1 of
Measurement Location: N Sound Level Meter	5A-N10 31	Field Calloration	Analyst B. VASQUEZ
Mode # AD		= LD CAL 200	Meteorological Data Model = Kestvel 3500 Time Ocs We
Sera = 447		= 5789	Se's =
Neighting & D Flat		(#3) 84 114	Freschaton Yes (explain) / 80
Response Sign (Fast (mp)		st 1/4 dB4	Wind Steady Gusty C2-
Aindscreen : Yas No (explain)	Post-Te		
Topo (at/Hilly		dinates (at 5LM location)"	Temp (F) 67 R4 A 837
Terrain HArd Soft Myad &	12 Sans 181 410 (16'	C W. 96' 14'55"	Bar Far (Hg Cloud Cover (N) 989
Loc D Start Time Stop Time	Metrics	Statistics	
CONTRACTOR OF SERVICE	4 Acc 6-10		Notes Events
51-10 11:10 11:40	65.3		dog bankin across M-51
	67.1		dog bankin across M-51
	66.1		rustling leves, crickets inser
	68.4		
	67.2		
	67.9	++	
	66.3		1
	68.2		
	67.0		
	66.6		
	67.7		
	67.8		
	65.0		14. 6.2. 1
	68.8	- I namana	4486Data - 006 Site Diagram
Roadway Name Dir.	11-51	compass	Site Diagram
Speed (post obs*)		10	
Number of Lanes			805
Width (pave row)			· · · · · · · · · · · · · · · · · · ·
1- or 2- wa/			
Grade		- 1	1
Bus Stops		1	THEE'S
Stoplights		10	~
Motorcycles		- 2	66
Automobiles	365		Tree ? . ASLA.
Medium Trucks	3	. 3.	208 C. 1984.
Heavy Trucks	4	-	V
Buses	2	1000	
Count duration		/	1-57
First contrast poem formation NO	30 m/s.	g Collegeor	Photos Taken? Yes / 1
Additional Notes Comments.			165/1
			4
· Karakaran		= -	
40 56 S0J/088 OFCE \$11		trafficing ops landscaping in sting is as and Skatches on Reverse or not	aves hidren playing dogs banking birds foodiang reads mediten de

Project Name MOOT (15-12/M	-51 P	roject # 6066 (6489 Date 9.24.2021 Page , of
Measurement Location. NS Sound Level Meter	H-NII	S/ -1/	for	Analyst B. Vasane 2
Mode = LD L	XT	Model = Z D	CAL 200	None = Kestrel 3500 Traces
Sera = 44 8		Sera'= 57	89	Sera =
Neighting Mac Fiet	Dal pratici	Leve (dB) 94		Frequitation Yes jexplain, No
Response Sou Fast Imp		Pre-Test 1/4	485	Wind Steady Gust, Q-
Mindspreen (As No (explain)		ost-Test	dBA.	Aug Wind Speed Direction - s/W
Toso Van Hily	, GE	S Coordinates (at 8	LW location (Ters F 55° 84 767
Terrain: Hord Soft Mixed Ago	Snow N: 41.º	48 6 W 8	6 15 17	Bar Par Ing Could Ocyer (%)
Lot O Start Time Stop Time	Metros	44 6	Statistics L	Notes Events
ST-11 09:30 09:50				interestionet RTE 12 & 13th s.
27 11 101.20 101.30				Influence toni 1 10 10 9 13 30
				<u> </u>
				1
			-	
			5000000	4414 Daha NO 1 Site Diagram:
Roadway Name Dir	RTE 12	13th St.	compass	Site Diagram
Speed (post obs*)	55			
Number of Lanes	# 6/W		V	- /
Width (pave'row)				
1- or 2- way				
Grade				
Bus Stops			1	
Stoplights	yes.		1	876 12
Motorcycles			1	1 21212
Automobiles				
Medium Trucks	100			120FL.
Heavy Trucks			1	1/1/
Buses			1	627-7 SLA
Count duration			1	Re.
 Fotogors have risten Yother than NAC84 	Sched eximated by Rad	or Dary Downer	-	Photos Taken? Yes /
Additional Notes Comments.				
1		_		ves children playing sogs carking biras (casi and reach mechanical

AECOM Acoustics and Noise Control Practice FIELD NOISE MEASUREMENT DATA FORM Project Name: MDOT Project #: 60666488 Date: 9/29/21 US-12/M-51 Measurement Location: 5T-12 Analyst: 6 1-1 Sound Level Meter Field Calibration Meteorological Data CXT Model # CAL 200 Model#: Kestre | 3500 Time Obs/Meas: Serial #: 4926 Serial #: 4637 Serial #: 2058303 9:32 Weighting(A) C / Flat Calibration Level (dB): 94 /614) Precipitation: Yes (explain) / No Response: Slow/ Fast / Impl Pre-Test - 0.03 dBA Wind: Steady / Gusty Calm Windscreen (Yes) No (explain) Post-Test - 0.00 dBA m/s / MPH Avg Wind Speed/Direction: Topo: Flat (Hilly) GPS Coordinates (at SLM location)^a Temp (°F): 67.7 RH (%): 68.4 Terrain: Hard / Soft (Mixed) Agg / Snow 41.8009730, -86.2548939 Bar Psr (Hg): 29. 22 Cloud Cover (%): 1000 Start Time Stop Time Metrics Notes/Events Lmax (hh:mm) (hh:mm) Lto L50 9:27 9:52 Runtime 9:30 71.0 65.9 9:35 9:40 64.7 69.5 72.5 9: 45 9:50 US-12 compass Site Diagram: Roadway Name/Dir. 45 Speed (post/obs*) Number of Lanes 4 Width (pave/row) 2 1- or 2- way Grade US/12 Bus Stops E.B. W. 13. C4 lanes) Stoplights Diso Motorcycles Automobiles 100 Medium Trucks 10 Heavy Trucks 15 16 Buses 93 102 SFR 20 Min Count duration 20 min - note coordinate system if other than NAD Photos Taken? (Yes) No Additional Notes/Comments: Audible Beeping from Crossing Signal Noise Sources (circle all that apply): distant aircraftroadway traffic)rail opsitandscapingrussting leaves brildren playing/dogs banking binds vocalizand insochamechanical Additional Notes and Sketches on Reverse of Indicated Separate Sheet(s) AECOM ANCP, Field Noise Measurement Form, Vers. 1.3 rev081816 File . 012

AECOM Acoustics and Noise Control Practice FIELD NOISE MEASUREMENT DATA FORM MDOT US-12/M-51 Project Name: Project #: 60666 41880ate: 9/21/21 of Measurement Location: Analyst: 6H Sound Level Meter Field Calibration Meteorological Data Model #: AL Model #: Kestral 390 Time Obs/Meas: Serial #: 4657 12:03 Serial #: 205 8303 Weighting A/C / Flat Calibration Level (dB): 94 (114) Precipitation: Yes (explain) No Response Slow / Fast / Impl Pre-Test + 0,12 dBA Wind: Steady / Gusty (Calm) Windscreen : (es) No (explain) m/s / MPH Post-Test - 0.03 dBA Avg Wind Speed/Direction: Topo (Flat) Hilly Temp (°F): 74/.6 RH (%): 75.2 GPS Coordinates (at SLM location)* Terrain: Hard / Soft / Mixed / Agg / Snow UL 796405, -86,24697 Bar Psr (Hg):29 .2 / Cloud Cover (%): 100 Start Time Stop Time Metrics Statistics Loc. ID Notes/Events (hh:mm) (hh:mm) Lmax Lon Leg Lta L₅₀ 12:02 12:27 Runtime 12:05 51.7 12:10 61.8 12:15 52.0 12:20 55.3 63.3 NYO compass Site Diagram: Roadway Name/Dir. M-51 wh. N Speed (post/obs*) 50 Number of Lanes 4 Width (pave/row) 1- or 2- way Grade Bus Stops NB Stoplights 5 Motorcycles 5 181 Automobiles Field Medium Trucks Heavy Trucks Buses Count duration 4-note coordinate system if other than NADA'. Speed estimated by Radar / Divergi / Observation Additional Notes/Comments: - Special ic NOBE from Auto Medic - Sporad ic Vehicle traffic in particing lot Photos Taken? (Yes) No Noise Sources (circle all that apply): distant aircrating adway trafficitall opsilandscaping outling leaves children playing logs banking ords vocalizing insects mechanical Additional Notes and Sketches on Reverse or Indicated Separate Sheet(s) AECOM ANCP, Field Noise Measurement Form, Vers. 1.3 rev081816

Project Name: MDOT	US-12/	M-51	Proj	ect#6	0666	488 Date 9 . 21 . 2021 Page 1 of 1 URA Analyst B. Vasquez
Sound Level Meter	V3H-3-	Fie	d Calibratic	4 10) lo He	Meteoro Zoical Data
Model = LD		Model #			00	Mode = Kestrel 3500 Time Ots We
Seria = 44			571			Sera A
Neighting N O Fat		ator Level (5				Preopitation Yes (explain) Q:
Response \$2 A Fast Imp			114		54	Wind Steady Gusty Cp
Mindscreen : Yas I No (exclain		Post-Test			84	Avg Wind Speed Director 18/ VPm
Topo Par/H/V		GPS Coordin	a'as (a', S.J.	flocation	12	Ter: 15 68' R- 85%
Terrain logical Soft Mixed A	C #1: /1	1"47'5	2 W: 86	15'	0"	Bar Par (Hg) Cloud Cover (%)
Start Time Stop Tim	e Met	ĊS .	S	121.51.09		Notes Events
The state of the variety	the second second	Lip	L.	de 1	40	
ST.13A12: 05 12:30		-		-		1 1 (2) 26 1 1 7
	56.8	+	-			giko nt 12:08 lis trale prossing
	68 8	-				" 12:4 by Jonk "
	62.1				-	1 (2.2 WS passing
	56.9			1		
	61.1					
	596					
	596	-				
	58.8					
	57.0	-		-		
	59.6	-	-			
	55.5		1			
	59.0					4486Deta.007
Roadway Name Dir	11-315			comp	888	Site Diagram:
Speed (postlobs*)				E4	9	_ 51
Number of Lanes	2		-		-	1
Width (pave row)				1	/	
1- or 2- way				11 1	1	
Grade	-			11 .		(3
Bus Stops			-	1	-	8
Stoplights	yes			1 .	1	100 yds.
Motorcycles	1			1:		E
Automobiles	234			1	1	
Medium Trucks				1	1	
Heavy Trucks	12			1		· V
Buses				1	510	1. 2 % SCM
Count duration				1		Res
FINDS poordings system flother than NA	34 *- Special mest	Pater Drives	Drever	1	-	Photos Taken? Yes / N
Additional Notes Comments						,

AECOM Acoustics and Noise Control Practice FIELD NOISE MEASUREMENT DATA FORM MDOT US-12/M-51 Project Name: Project #: 60666 488 Date: Measurement Location: ST-14 Analyst: Sound Level Met Field Calibration Meteorological Data Model # LD (Model #. [AL 200 Model # Gestrel 3500 Time Obs/Meas: Serial #: 4637 11-20 Serial #: Serial #: 2058303 Weighting: A / C / Flat Calibration Level (dB): 94 / 114 Precipitation: Yes (explain) / No Pre-Test -0.03 dBA Response (Slow) Fast / Impl Wind Steady / Gusty / Calm Windscreen (Yes No (explain) Post-Test +0.03 dBA Avg Wind Speed/Direction: 2 m/s/ MPH Topo: Flat (Hilly) Terrain: Hard (Soft) Mixed / Agg / Snow GPS Coordinates (at SLM location) Temp (°F): 57.5 RH (%): 41,8007173, -86.24286 Bar Psr (Hg): 29 27 Cloud Cover (%): Start Time Stop Time Metrics Statistics Loc. ID Notes/Events (hh:mm) (hh:mm) L_{max} Link L10 Lso 11:15 11:40 11:20 67.8 11:25 70:3 11:50 68.3 11:35 69.9 compass Site Diagram: Roadway Name/Dir. 05-12 50 Speed (post/obs*) Number of Lanes 4 Width (pave/row) US-12 1- or 2- way Grade Bus Stops Stoplights Motorcycles SFR Automobiles Medium Trucks Heavy Trucks Ava. Greendale Buses Count duration note coordinate system if other than NAD64 Photos Taken? (Yes) No - Vehicle Courts from Corners on US-12 Noise Sources (circle oil that apply): distant aircraft gadway trafficial ops and scaping fustling leaves thildren playing logs banking birds vocalizing insects Additional Notes and Sketches on Reverse or Indicated Separate Sheet(s) AECOM ANCP, Field Noise Measurement Form, Vers. 1.3 rev081816

Equipment Calibration Certificates

CERTIFICATE OF CALIBRATION # 26401-1 FOR LARSON DAVIS PRECISION INTEGRATING SOUND LEVEL METER

Model LxT1

Serial No. 0004926

ID No. 4926

With Microphone 377C20

Serial No. 151721

With Preamplifier PRMLxT1L

Serial No. 042680

Customer: AECOM

San Diego, CA 92101

P.O. No. Credit Card

was tested and met Larson Davis specifications at the points tested and as outlined in ANSI S1.4-1983 Type 1; IEC 61672-2002 Class1; 60651-2001 Type 1

on 07 JUN 2021

BY HAROLD LYNCH Service Manager

As received and as left condition: Within Specification.

Re-calibration due on: 07 JUN 2022

	References*			
Mfg.	Type	Serial No.	Cal Date	Due Date
B&K	1051	1777523	28 SEP 2020	28 SEP 2021
B&K	2636	1423390	04 JAN 2021	04 JAN 2022
B&K	4226	3274134	30 NOV 2020	30 NOV 2021
B&K	4231	1770857	10 SEP 2020	10 SEP 2021
HP	34401A	MY45023668	28 JAN 2021	28 JAN 2022
HP	3458A	2823A07179	21 JUL 2020	21 JUL 2021
and	d ISO 17025, ISO	iance with ANSI, NCSI 9001:2015 Certification ble to NIST (National Inst		anology).

Note: For calibration data see enclosed pages.

The data represent both "as found" and "as left" conditions.

Reference Test Procedure: ACCT Procedure LxT-831 Version 0.5.1.

Temperature Relative Humidity Barometric Pressure 23°C 41 % 986.52 hPa

Note: This calibration report shall not be reproduced, except in full, without written consent by Odin Metrology, Inc. Signed: Lossef Superior Signed:

ODIN METROLOGY, INC.

CALIBRATION OF SOUND & VIBRATION INSTRUMENTATION
3533 OLD CONEJO ROAD, SUITE 125 THOUSAND OAKS CA 91320
PHONE: (805) 375-0830 FAX: (805) 375-0405

Doc. Rev. 16 Feb 2018

Page 1 of 12

Odin Metrology, Inc. Calibration of Sound & Vibration Instruments

Certificate Number: 26401-6

Certificate of Calibration for Larson Davis Calibrator

This calibration is performed by comparison with measurement reference standard microphone:

Type No.	4134
Serial No.	1315901
Calibrated by	HL
Cal Date	24 MAR 2021
Due Date	24 MAR 2022

- Estimated uncertainty of comparison: ± 0.05 dB
- Estimated uncertainty of calibration service for standard pistonphone: ± 0.06 dB
- Total uncertainty: $\sqrt{a^2 + b^2} = \pm 0.08 dB$
- Expanded uncertainty (coverage factor k = 2 for 95% confidence level): = ± 0.16 dB

This acoustic calibrator has been calibrated using standards with values traceable to the National Institute of Standards and Technology. This calibration is traceable to NIST Test Number 683/289533-17.

CONDITION	N OF TEST		
Ambient Pressure	989.33	hPa	
Temperature	23	°C	
Relative Humidity	41	%	
Date of Calibration	08 JUN	2021	
Re-calibration due on	08 JUN 2022		

The calibration of this acoustic calibrator was performed using a test system conforming to the requirements of ANSI/NCSLZ540-1, 1994, ISO 17025, ISO 9001:2015, Certification NQA No. 11252.

Calibration procedure: OM-P-1001-Acoustic_Calibrator, Rev. 1.0 20130522.

Calibration performed by

Harold Lynch, Service Manager

ODIN METROLOGY, INC. 3533 OLD CONEJO ROAD, SUITE 125 THOUSAND OAKS, CA 91320 PHONE: (805) 375-0830; FAX: (805) 375-0405 Calibrator type CAL200 Serial no. 4637 Submitted by **AECOM** San Diego, CA 92101

Purchase order no. Credit Card

Asset no. N/A

This calibrator has been found to perform within the specifications listed below at the normalized conditions stated.

SPL produced in coupler terminated by a loading volume of a ½" microphone	94.0 ± 0.2 dB 114 ± 0.2 dB
Frequency	1,000 Hz ± 1%
Distortion	< 2%
At 1.013 hPa, 23°C, and 6	5% relative humidity

PERFORMA	NCE AS RECEIVED)	
Frequency	1000.1	Hz	
SPL (94 dB)	93.97	dB	
SPL (114 dB)	113.97	dB	
Distortion (at 94 dB)	0.3	%	
Battery Voltage	9.4	V	

Was adjustment performed?	No
Were batteries replaced?	No

FINAL PERFORMANCE								
Frequency	1000.1	Hz						
SPL (94 dB)	93.97	dB						
SPL (114 dB)	113.97	dB						
Distortion (at 94 dB)	0.3	%						

Note: This calibrator was within manufacturer's specifications as received.

Note: This calibration report shall not be reproduced, except in full, without written consent of Odin Metrology, Inc.

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CERTIFICATE OF CALIBRATION # 26354-7 FOR LARSON DAVIS PRECISION INTEGRATING SOUND LEVEL METER

Model LxT1 Serial No. 0004486

ID No. N/A

With Microphone 377B20 Serial No. 149336
With Preamplifier PRMLxT1L Serial No. 029355

Customer: AECOM

San Diego, CA 92101 P.O. No. Credit Card

was tested and met Larson Davis specifications at the points tested and as outlined in ANSI S1.4-1983 Type 1; IEC 61672-2002 Class1; 60651-2001 Type 1

on 06 MAY 2021

BY HAROLD LYNCH Service Manager

As received and as left condition: Within Specification. Re-calibration due on: 06 MAY 2022

Certified I	References*			
Mfg.	Type	Serial No.	Cal Date	Due Date
B&K	1051	1777523	28 SEP 2020	28 SEP 2021
B&K	2636	1423390	04 JAN 2021	04 JAN 2022
B&K	4226	3274134	30 NOV 2020	30 NOV 2021
B&K	4231	1770857	10 SEP 2020	10 SEP 2021
HP	34401A	MY45023668	28 JAN 2021	28 JAN 2022
HP	3458A	2823A07179	21 JUL 2020	21 JUL 2021
		iance with ANSI, NCSI 9001:2015 Certification		
			itute of Standards and Tech	nnology).

Note: For calibration data see enclosed pages.

The data represent both "as found" and "as left" conditions.

Reference Test Procedure: ACCT Procedure LxT-831 Version 0.5.1.

Temperature	Relative Humidity	Barometric Pressure	
23°C	37 %	990.38 hPa	

Note: This calibration report shall not be reproduced, except in full, without written consent by Odin Metrology, Inc.
Signed:

ODIN METROLOGY, INC.

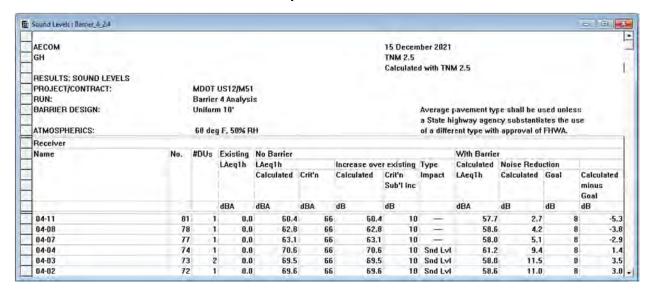
CALIBRATION OF SOUND & VIBRATION INSTRUMENTATION
3533 OLD CONEJO ROAD, SUITE 125 THOUSAND OAKS CA 91320
PHONE: (805) 375-0830 FAX: (805) 375-0405

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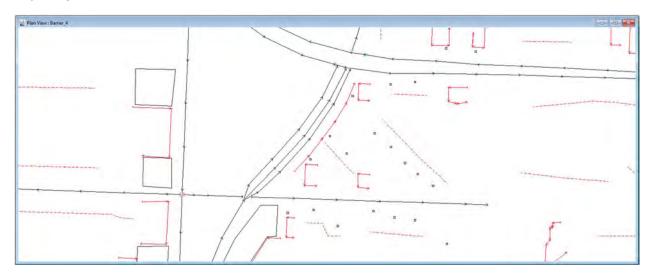
Appendix B Sample TNM Input/Output Files

Sample TNM output tables are provided for CNE 4 Abatement analysis. Additional input and output files are available upon request.

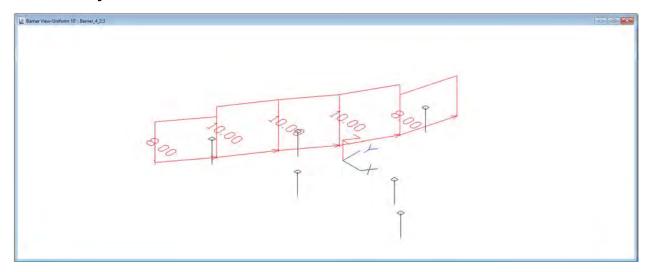
CNE 4 TNM Sound Level Prediction Output Table



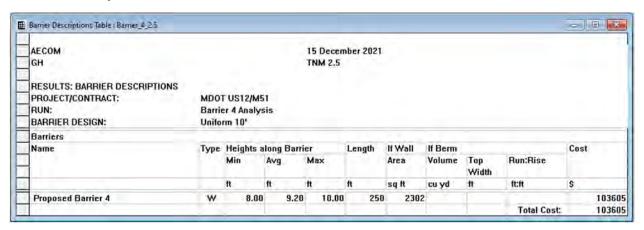
Plan View



Barrier Analysis Screenshot



Barrier Description Table



Appendix C Predicted Noise Levels and Impacts

Table C-1 Loudest Hour Noise Levels, Leq(1h), dBA

Receptor Number	Land Use	Activity Category	Units	FHWA/MDOT NAC	Existing	Build	Change
			CN	IE 1			
01-01	Residential	В	1	66	61	66	5
01-02	Residential	В	1	66	64	69	4
01-03	Residential	В	1	66	63	68	6
01-04	Residential	В	1	66	63	69	5
01-05	Residential	В	1	66	61	64	3
01-06	Residential	В	1	66	61	64	3
01-07	Residential	В	1	66	62	64	2
01-08	Residential	В	<u> </u>	66	62	64	2
01-09	Residential	В	<u> </u>	66	62	64	2
01-10	Residential	В	<u>.</u> 1	66	61	63	2
01-11	Residential	В	1	66	62	64	2
01-11	Residential	В	<u>'</u> 1	66	63	66	2
01-12	Residential	В	1	66	65	68	2
01-14	Residential	В	1	66	66	68	2
01-15	Residential	В	1	66	61	62	1
01-16	Residential	В	1	66	61	61	0
01-17	Residential	В	1	66	65	66	1
01-18	Residential	В	1	66	66	66	1
01-19	Residential	В	1	66	63	63	1
01-20	Residential	В	1	66	62	63	1
01-21	Residential	В	1	66	62	62	1
01-22	Residential	В	1	66	61	61	1
01-23	Residential	В	1	66	56	57	1
01-24	Residential	В	1	66	55	55	1
01-25	Residential	В	1	66	56	56	1
01-26	Residential	В	1	66	58	59	1
01-27	Residential	В	1	66	58	59	1
01-28	Residential	В	1	66	58	59	1
01-29	Residential	В	1	66	61	62	1
01-30	Residential	В	1	66	61	61	1
01-31	Residential	В	<u> </u>	66	55	56	1
01-32	Residential	В	1	66	53	54	1
01-33	Residential	В	<u> </u>	66	56	56	0
01-34	Residential	В		66	56	57	0
01-35	Residential	В	<u>'</u>	66	58	58	0
01-36	Residential	В	1	66	59	61	2
01-36	Residential	В	<u> </u>	66	60	61	2
		В	<u> </u>				1
01-38	Residential	_	· · · · · · · · · · · · · · · · · · ·	66	60	62	· ·
01-39	Residential	В	1	66	60	61	1
01-40	Residential	В	1	66	58	59	1
01-41	Residential	В	1	66	57	58	1
01-42	Residential	В	1	66	57	58	1
01-43	Residential	В	1	66	56	58	1
01-44	Residential	В	1	66	57	58	2
01-45	Residential	В	1	66	57	58	2
01-46	Residential	В	1	66	57	60	2
01-47	Residential	В	1	66	58	60	2
01-48	Residential	В	1	66	58	60	2
01-49	Residential	В	1	66	58	60	2
01-50	Residential	В	1	66	57	59	2
01-51	Residential	В	1	66	58	60	2
01-52	Residential	В	1	66	58	60	2
01-53	Residential	В	1	66	57	60	2

Receptor Number	Land Use	Activity Category	Units	FHWA/MDOT NAC	Existing	Build	Change
01-54	Residential	В	1	66	56	58	2
01-55	Residential	В	1	66	53	55	2
01-56	Residential	В	1	66	54	56	2
			CN	IE 2			
	Commercial						
02-01	(Restaurant)	E	0	71	67	68	1
02-02	Residential	В	1	66	54	55	1
02-03	Residential	В	6	66	57	57	1
02-04	Residential	В	1	66	60	61	1
02-05	Residential	В	1	66	53	54	1
02-06	Residential	В	1	66	54	55	1
02-07	Residential	В	1	66	57	58	1
02-08	Residential	В	1	66	53	53	1
02-09	Residential	В	11	66	53	53	1
02-10	Residential	В	1	66	52	53	1
02-11	Residential	В	1	66	54	55	1
02-12	Residential	В	1	66	52	52	1
	A atio Ct		CN	IE 3			
02.04	Active Sport		0	66	E7	E7	4
03-01 03-02	Area Cemetery	C	0	66	57 61	57 62	1 1
03-02	Cemetery	C	1	66	68	69	1
03-03	Cemetery	C	<u></u> 1	66	68	69	1
03-04	Cemetery	C	<u>'</u> 1	66	68	69	1
03-06	Cemetery	C	1	66	68	69	1
03-07	Cemetery	C	1	66	68	69	1
03-08	Cemetery	C	<u>.</u> 1	66	69	69	1
03-09	Cemetery	C	<u>.</u> 1	66	69	69	1
03-10	Cemetery	C	1	66	69	70	1
00.10				IE 4			-
04-01	Residential	В	1	66	66	67	1
04-02	Residential	В	1	66	69	70	1
04-03	Residential	В	2	66	69	70	1
04-04	Residential	В	1	66	70	71	1
04-05	Residential	В	1	66	60	60	0
04-06	Residential	В	1	66	64	64	0
04-07	Residential	В	1	66	63	63	1
04-08	Residential	В	1	66	62	63	1
04-09	Residential	В	1	66	71	71	0
04-10	Residential	В	1	66	59	59	0
04-11	Residential	В	1	66	60	60	0
04-12	Residential	В	1	66	72	72	0
04-13	Residential	В	1	66	60	60	0
04-14	Residential	В	11	66	59	59	0
04-15	Residential	В	1	66	58	58	0
04-16	Residential	В	11	66	58	59	0
04-17	Residential	В	1 1	66	58	58	0
04-18	Residential	В	1 1	66	58	58	0
04-19	Residential	В	1	66 IE 5	56	56	0
05.04	Posidontial	В			68	68	0
05-01 05-02	Residential Residential	В	1 1	66 66	70	68 70	0
05-02	Residential	В	<u></u> 1	66	64	65	0
05-03	Residential	В	<u></u> 1	66	61	62	0
05-04	Residential	В	1	66	65	65	0
05-06	Residential	В	1	66	66	66	0
05-07	Residential	В	1	66	69	69	0
05-07	Residential	В	1	66	65	65	0
05-09	Residential	В	1	66	56	56	0
05-10	Residential	В	1	66	58	58	0
00-10	Residential	ا	<u>'</u>	1 30	00		

Receptor Number	Land Use	Activity Category	Units	FHWA/MDOT NAC	Existing	Build	Change
05-11	Residential	В	1	66	53	53	0
05-12	Residential	В	1	66	57	57	0
05-13	Residential	В	1	66	51	52	0
05-14	Residential	В	1	66	50	51	0
05-15	Residential	В	1	66	46	46	0
05-16	Residential	В	1	66	51	51	0
05-17	Residential	В	1	66	56	56	0
05-18	Residential	В	1	66	60	60	0
05-19	Residential	В	1	66	59	60	0
05-20	Residential	В	1	66	55	55	0
05-21	Residential	В	1	66	55	55	0
05-22	Residential	В	1	66	59	59	0
05-23	Residential	В	1	66	53	53	0
05-24	Residential	В	1	66	50	51	0
05-25	Residential	В	1	66	49	49	0
05-26	Residential	В	1	66	47	48	0
			CN	IE 6	'		·
06-01	Residential	В	1	66	64	64	0
06-02	Residential	В	1	66	61	62	1
06-03	Residential	В	1	66	60	60	1
06-04	Residential	В	<u>.</u> 1	66	61	61	0
06-05	Residential	В	1	66	59	59	1
06-06	Residential	В	<u>.</u> 1	66	62	62	0
06-07	Residential	В	1	66	62	63	0
06-08	Residential	В	1	66	61	62	1
06-09	Residential	В	'	66	60	60	1
06-10	Residential	В	1	66	61	61	1
06-10	Residential	В	1	66	59	59	1
06-11	Residential	В	1	66	52	53	1
06-12		В					
06-13	Residential	В	1 1	66	52 52	53	1 1
06-14	Residential	В	<u></u> 1	66	52	53 52	1
	Residential						
06-16 06-17	Residential	B B	1	66 66	51 51	52 51	1
	Residential		11				1
06-18	Residential	В	11	66	58	59	1
06-19	Residential	В	1	66	58	59	1
06-20	Residential	В	1	66	58	59	0
06-21	Residential	В	1	66	56	56	0
06-22	Residential	В	1	66	61	62	0
06-23	Residential	В	1	66	60	61	0
06-24	Residential	В	11	66	57	57	0
06-25	Residential	В	1	66	59	59	0
06-26	Residential	В	11	66	60	60	0
06-27	Residential	В	1	66	60	60	0
06-28	Residential	В	1	66	56	56	0
06-29	Residential	В	1	66	55	55	0
06-30	Residential	В	1	66	59	59	0
06-31	Residential	В	1	66	60	61	0
06-32	Residential	В	1	66	57	58	0
06-33	Residential	В	1	66	56	57	1
06-34	Residential	В	11	66	57	58	1
06-35	Residential	В	1	66	50	50	1
06-36	Residential	В	1	66	50	51	1
06-37	Residential	В	1	66	51	51	1
06-38	Residential	В	1	66	50	51	1
06-39	Residential	В	1	66	59	59	0
06-40	Residential	В	1	66	59	60	0
06-41	Residential	В	1	66	54	54	0
06-42	Residential	В	1	66	55	55	0
06-43	Residential	В	1	66	59	59	0

Receptor Number	Land Use	Activity Category	Units	FHWA/MDOT NAC	Existing	Build	Change
06-44	Residential	В	1	66	63	63	0
06-45	Residential	В	1	66	65	65	0
06-46	Residential	В	1	66	61	61	0
06-47	Residential	В	1	66	57	58	0
06-48	Residential	В	1	66	54	54	0
06-49	Residential	В	1	66	57	57	0
06-50	Residential	В	1	66	58	59	0
06-51	Residential	В	1	66	54	55	0
06-52	Residential	В	1	66	54	55	0
			CN	E 7			
	Commercial	_	_				_
07-01	(Restaurant)	E	0	71	69	69	1
22.24	5		CN				1
08-01	Residential	В	1	66	60	60	1
08-02	Residential	В	1	66	58	59	2
08-03	Trail	С	0	66	58	60	2
08-04	Trail	С	0	66	64	64	0
08-05	Residential	B C	1	66	66	67	1
08-06 08-07	Church Residential	В	0	66 66	63 60	63 59	-1
UO-U/	Residential	D	CN		δU	59	-1
09-01	Residential	В	1 1	E 9	66	67	1
09-01	Residential	В	1	66	61	61	1
09-03	Residential	В	1	66	57	58	1
09-04	Residential	В	1	66	56	56	1
09-05	Residential	В	1	66	56	56	1
09-06	Residential	В	1	66	56	57	0
09-07	Residential	В	1	66	68	69	1
09-08	Residential	В	1	66	65	65	0
09-09	Residential	В	1	66	66	66	0
09-10	Residential	В	1	66	65	65	0
09-11	Residential	В	1	66	64	64	0
09-12	Residential	В	1	66	63	64	0
09-13	Residential	В	1	66	63	64	1
09-14	Residential	В	1	66	64	64	1
			CNE 10 (No				
			CNE				
11-01	Residential	В	1	66	54	55	1
11-02	Residential	В	1	66	55	56	1
11-03	Residential	В	1	66	56	56	1
11-04	Residential	<u>В</u> В	1	66 66	56 56	57 57	1
11-05	Residential Residential	В	1	66		57 55	1
11-06 11-07	Residential	В	1	66	55 55	55 	1 1
11-07	Residential	В	1	66	57	57	1
11-08	Residential	В	1	66	56	57	1
11-09	Residential	В	1	66	54	55	1 1
11-10	Residential	В	1	66	53	55	1
11-12	Residential	В	1	66	53	53	1
	1 (Sugaritial		CNE				•
12-01	Residential	В	1	66	66	66	0
12-02	Residential	В	1	66	66	66	0
12-03	Residential	В	1	66	66	67	0
12-04	Residential	В	1	66	61	63	3
12-05	Residential	В	1	66	68	71	3
12-06	Residential	В	1	66	68	70	3
12-07	Residential	В	1	66	69	70	1
12-08	Residential	В	1	66	57	58	0
12-09	Residential	В	1	66	58	59	0
12-10	Residential	В	1	66	60	62	2

Receptor Number	Land Use	Activity Category	Units	FHWA/MDOT NAC	Existing	Build	Change
12-11	Residential	В	1	66	60	62	2
12-12	Residential	В	1	66	60	60	1
12-13	Residential	В	1	66	61	61	1
12-14	Residential	В	1	66	61	62	1
12-15	Residential	В	1	66	60	61	1
12-16	Residential	В	1	66	59	60	1
12-17	Residential	В	1	66	59	59	1
12-18	Residential	В	1	66	59	60	1
12-19	Residential	В	1	66	59	61	2
12-20	Residential	В	1	66	59	61	2
12-21	Residential	В	1	66	63	64	1
12-22	Residential	В	1	66	54	55	0
12-23	Residential	В	1	66	54	54	0
12-24	Residential	В	1	66	54	54	0
12-25	Residential	В	1	66	56	56	0
12-26	Residential	В	1	66	55	55	0
12-27	Residential	В	1	66	57	58	0
12-28	Residential	В	1	66	57	57	1
12-29	Residential	В	1	66	54	55	1
12-30	Residential	В	1	66	55	57	1
12-31	Residential	В	1	66	55	57	2
12-32	Residential	В	1	66	58	60	1

Note: Bolded values represent noise impacts.

Appendix D Noise Barrier Analysis Detail

Table D-1 Noise Barrier Analysis, Receiver Level Detail

Receptor Number	Land Use	Category	Units	FHWA/MDOT NAC	Build	Noise Level w/Barr	Noise Reduction	Benefit?
	,			Wall 1A				
01-01	Residential	В	1	66	66	61	5	Υ
01-02	Residential	В	1	66	69	61	8	Υ
01-03	Residential	В	1	66	68	59	10	Υ
01-04	Residential	В	1	66	69	59	10	Υ
01-05	Residential	В	1	66	64	57	7	Υ
01-06	Residential	В	1	66	64	57	6	Y
01-07	Residential	В	1	66	64	61	3	
01-08	Residential	В	1	66	64	62	2	
01-09	Residential	В	1	66	64	62	2	
01-10	Residential	В	1	66	63	62	1	
01-11	Residential	В	1	66	64	62	3	
01-12	Residential	В	1	66	66	59	6	Υ
01-13	Residential	В	1	66	68	58	9	Υ
01-14	Residential	В	1	66	68	58	10	Υ
				Wall 1B				
01-16	Residential	В	1	66	61	60	1	
01-17	Residential	В	1	66	66	62	4	
01-18	Residential	В	1	66	66	59	7	Υ
01-19	Residential	В	1	66	63	59	4	
01-20	Residential	В	1	66	63	60	3	
01-21	Residential	В	1	66	62	61	1	
01-22	Residential	В	1	66	61	61	1	
01-33	Residential	В	1	66	56	54	2	
01-34	Residential	В	1	66	57	55	2	
01-35	Residential	В	1	66	58	57	1	
				Wall 3				
03-03	Cemetery	С	1	66	69	64	5	Υ
03-04	Cemetery	С	1	66	69	62	7	Υ
03-05	Cemetery	С	1	66	69	62	8	Υ
03-06	Cemetery	С	1	66	69	61	8	Υ
03-07	Cemetery	С	1	66	69	60	10	Υ
03-08	Cemetery	С	1	66	69	61	8	Υ
03-09	Cemetery	С	1	66	69	63	7	Υ
03-10	Cemetery	С	1	66	70	64	5	Υ
				Wall 4				
04-02	Residential	В	1	66	70	59	11	Υ
04-03	Residential	В	2	66	70	58	12	Υ
04-04	Residential	В	1	66	71	61	9	Υ
04-07	Residential	В	1	66	63	58	5	Υ
04-08	Residential	В	1	66	63	59	4	
04-11	Residential	В	1	66	60	58	3	
				Wall 5				
05-06	Residential	В	1	66	66	62	5	Υ
05-07	Residential	В	1	66	69	59	10	Υ

Receptor Number	Land Use	Category	Units	FHWA/MDOT NAC	Build	Noise Level w/Barr	Noise Reduction	Benefit?
12-02	Residential	В	1	66	66	65	0	
12-03	Residential	В	1	66	67	66	0	
12-04	Residential	В	1	66	63	62	1	
12-05	Residential	В	1	66	71	65	6	Y
12-06	Residential	В	1	66	70	60	10	Y
12-09	Residential	В	1	66	59	58	0	
12-10	Residential	В	1	66	62	60	2	
12-11	Residential	В	1	66	62	60	2	
12-12	Residential	В	1	66	60	59	1	
12-13	Residential	В	1	66	61	60	2	
12-14	Residential	В	1	66	62	60	2	
12-15	Residential	В	1	66	61	59	2	
12-16	Residential	В	1	66	60	58	2	
12-17	Residential	В	1	66	59	58	2	
12-18	Residential	В	1	66	60	58	2	
12-19	Residential	В	1	66	61	60	1	
12-20	Residential	В	1	66	61	61	0	
12-27	Residential	В	1	66	58	57	0	
12-28	Residential	В	1	66	57	57	1	
12-29	Residential	В	1	66	55	53	1	